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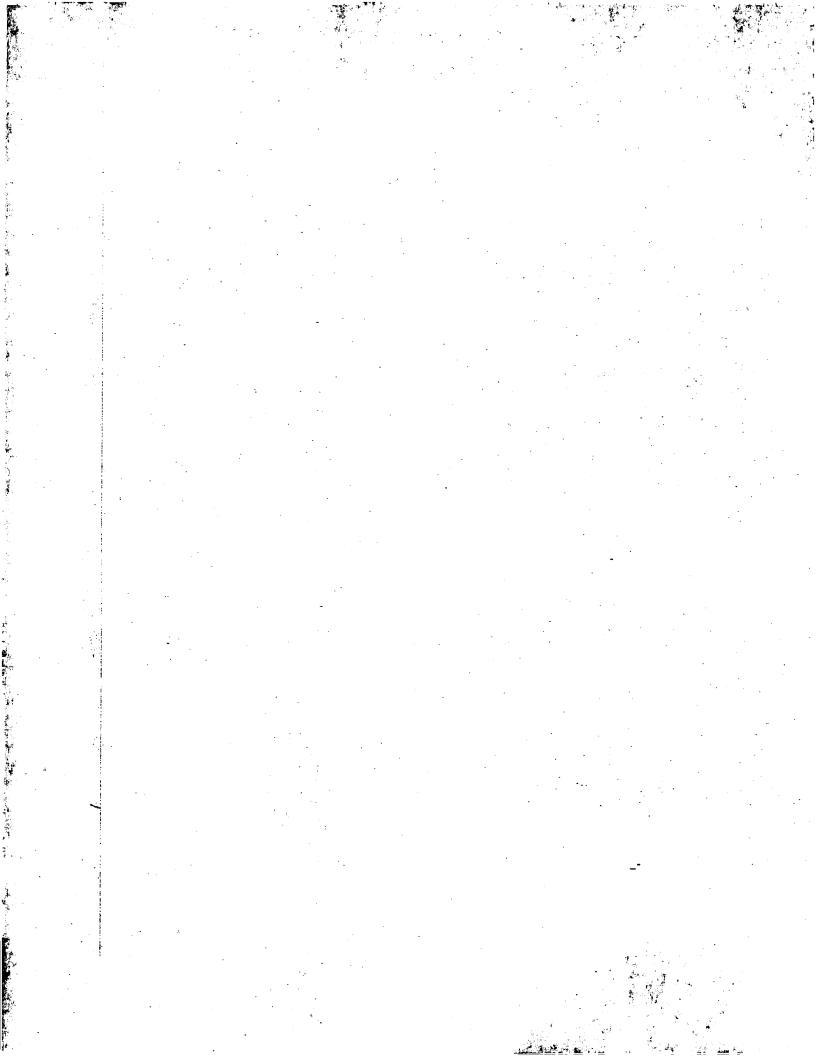
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(54) Title: CATALYTIC CELLULIGNIN FUEL

(57) Abstract: The present invention relates to a catalytic cellulignin fuel obtained by a biomass pre-hydrolysis process and that is composed of cellulose and globulized lignin with a specific surface of about 1.5 - 2.5 m2/g. The cellulignin fuel according to the invention may be ground down to particles smaller than 250 µm and has a combustion heat value that can reach up to 18 - 20 MJ/kg and an ignition time equal to or shorter than 20 ms (0.02s).



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Title: "CATALYTIC CELLULIGNIN FUEL"

#### Field of the Invention

The present invention relates to a new fuel obtained from biomass.

#### Background of the invention

The energy obtained from biomass is highly positive from the point of view of energy. For instance, the energetic efficiency of the so-called short-rotation biomass is 89.5%, and the rate of liquid energy is 9.48 times higher. However, in spite of this fantastic energetic efficiency, biomass cannot compete with fossil fuels due to the high costs resulting from the large number of steps required to produce it and also due to the difficulty in handling the raw biomass, which renders it not very practical.

The following points related to the process for producing biomass should be taken into account: 1) planting and cultivation (propagation); 2) expenses with nutrients (fertilization); 3) exposure to the sun; 4) temperature; 5) precipitation; 6) conditions of soil and water; 7) harvesting method; 8) resistance to diseases; 9) competition in the area with production of foodstuffs, pastures and fibers; 10) area availability; 11) transport of the raw biomass.

Biomasses are composed of cellulose, hemicellulose and lignin, the composition being exemplified in Table 1, and microstructure according to figure 1.

Table 1

Cellular wall	Typical	Composition - Pine	e (166 (20)
	hemicellulose	cellulose	lignin
M - middle Iamelia	-	•	3.0
o - primary wall	1,4	0,7	8.4
S - secondary wall		·	
S1	3,7	6,13	10,5
\$2	18,4	2,7	9.1
\$3	5,2	0,8	
Total	28,7.	40,3	31.8

The cellular walls are composed of macrofibrillae, microfibillae, micellae and cellulose molecules. The nuclei of the cells (cytoplasm) is composed of aqueous solutions. The following formulas represent the approximate estimates of the specific surface (area per unit of mass) of the biomass in the hypothesis of its microstructure being completely released.

1- Geometry with a Square section and length I (S and M: cell surface and cell mass).

$$S = 4bl; M = 4ble\rho : \frac{S}{M} = \frac{4bl}{4ble\rho} = \frac{1}{e\rho}$$

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broadness of the cell

 $b = 10 \mu m$ 

thickness of the cell wall:

e = 1.0µm

 $\rho$  = 1.5 g/cm<sup>3</sup>

= 1.5 X 10° g/m<sup>3</sup>

2. Specific area of the macrofibrillae, microfibrilla, miscellae and cellulose molecules.

$$S = \pi \phi l; M = \frac{\pi \phi^2}{4} l \rho : \frac{S}{M} = \frac{\pi \phi l}{\frac{\pi \phi^2}{4} l \rho} = \frac{4}{\phi \rho}$$

2.a - Specific area of the macrofibrilla (φ = 50nm; Macropores>50nm)

$$\frac{S}{M} = \frac{4}{50 \times 10^{-9} \times 1.5 \times 10^6} = 53m^2 / g$$

2.b - Specific area of the microfibrillae ( $\phi$ =50/4 = 12,5nm; Mesopores 2nm

5 <φ<50nm)

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$$\frac{S}{M} = \frac{4}{12.5 \times 10^{-9} \times 1.5 \times 10^{-4}} = 213m^2/g$$

2.c - Specific area of the miscella ( $\phi$  = (12.5/4)nm = 3,1nm; Micropores  $\phi$  <2.0nm)

$$\frac{S}{M} = \frac{4}{3.1 \times 10^{-9} \times 1.5 \times 10^6} = 860 m^2 / g$$

10 2.d - Specific area of the molecules of cellulose (3,1/6)nm = 0,517nm)

$$\frac{S}{M} = \frac{1}{0.517 \times 10^{-9} \times 1.5 \times 10^6} = 1290 m^2 / g$$

$$N = 1 + 6 \sum_{i=0}^{n} ni = 1$$
,  $(1 + 6 = 7)$ ,  $(1 + 6 + 12 = 19)$ ,  $(1 + 6 + 12 + 18 = 37)$ .

The theoretical specific area for the cell is of about 0.7m<sup>2</sup>/g, of about 50m2/g for the macrofibrillae, of about 200m2/g for the microfibrillae, of about 900m2/g for the miscealla, and of about 1300m2/g for the molecules.

As far as solid fuels are concerned, their conventional combustion comprises 5 zones: first non-reactive solid zone (heating and drying), second reaction zone of condensed phase (solid pyrolysis), third reaction zone of gaseous phase (pyrolysis of gaseous phase and oxidation), fourth primary combustion zone (gaseous phase), fifth post-flame reaction zone (secondary combustion). The specific kinetics and reactions of each zone is not completely known yet.

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Figure 2 illustrates the conceptual model of conventional combustion for wood. Wood is anisotropic and hygroscopic, and its fibers (tracheids) are hollow and have a length of from 3.5 to 7.0mm in soft wood, and from 1 to 2 mm in hard wood. The linked water is of about 23%, and the total moisture reaches 75%. Cellulose, hemicellulose and lignin behave as polyalcohols wherein the main functional group is the OH group. Cellulose is a linear polysaccharide of anhydrous glucose with  $1 \rightarrow 4-\beta$  glucoside bonds. After oxidation, the functional groups are carbonylic, ketone and carboxylic groups. On the other hand, hemicellulose is a polysaccharide with branched chain, the main components of which are 4-0-methylglucoroxylanes in hard wood and glucomanes in soft wood. The main functional groups thereof are carboxylic, methylic and hydroxylic groups. Lignin, on the other hand, is a tridimensional backbone of 4 or more substituted phenylpropane units. The basic constitutive blocks are guayaquil alcohols (soft wood) and seringyl alcohol (for the two types of wood), and the dominant bonds are  $\beta$ -0-4.

The structures of cellulose and lignin are highly oxygenated and the location of the functional groups is useful in understanding the mechanisms of pyrolysis and oxidation.

For the purpose of comparison, it is observed that the structure of the mineral coal is aromatic, it has few hydroxylic functional groups and  $\beta$ -0-4 bonds. Nitrogen and sulfur are part of the structural rings with little nitrogen existing in the amine form. The fact that the oxygen content is very low in coals when compared with wood is highly significant, since it imparts greater reactivity to the latter.

In the conventional combustion of wood the drying stage involves, in fact, 4 steps, namely 1) energy required for heating the wood up to 100° C (373°K) = 0.08 X 100 X (1 - TU) kJ/kg, wherein TU is the moisture content (percentage); 2) energy required for heating water = 4.2 X 100 kJ/kg; 3) energy required for vaporizing the water = 2.26 MJ/kg; and 4) energy required for releasing the linked water 15.5 X TU kJ/kg (average). The predominant value is the energy from vaporization of water.

The heating stage comprises three factors that have significant influence: the first one is the energy for heating up to the pyrolysis temperature (500 - 625 °K); the wood specific heat is 1113 J/g at 273 ° K and 1598 J/g at 373 °K, while the specific heat of the wood with 35% of moisture is 2.343 J/g at 300 °K. Secondly, there is the influence of the moisture preventing the particle core be heated up to the tem-

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perature at which water is evaporated and establishing the reaction states. The third factor of influence is the moisture in the increase of the thermal conductivity of the wood particle, which may at most double its value. In addition to its influence on the drying and heating, moisture also causes significant effects on the solid state pyrolysis

The next stage is the solid pyrolysis step. In this combustion zone, reactions of cleavage of the molecules into gaseous fragment and condensation reactions prevail, whereby coal is produced (tar resulting into 3 final fractions: a gaseous one, a liquid one, and a solid one - coal). The pyrolysis temperatures are: hemicellulose (500 - 600 ° K), cellulose (600 - 650 ° K) and lignin (500 - 773 K). Table 2 shows the pyrolysis products from cellulose and xylan, with a high tar content that causes a secondary combustion close to the oils for the wood.

Table 2: Pyrolysis Products from Cellulose (873 °K) and Xylan (773 °K)

Product	Cellulose (% P)	Xyilan (% P)
Acetaldehyde	1,5	2.4
Acetone Propinaldehyde	0,0	0,3
Furanics	0,7	Tr
Propenol	0,8	0,0
Methanol	1,1	1,3
2-Methylfuran	Tr	0,0
2,3-Butanedione	2,0	Tr
1-Hydroxy-2-Propan glycoxal	2,8	0,4
Acetic acid	1,0	1,5
2-Furaldehyde	1,3	4,5
5-Methyl-2-Furaldehyde	0,5	0,0
CO,	6,0	8.0
H₂O	11,0	7,0
Coal	5,0	10,0
Tar	66,0	64,0

Tr = trace

The opening of aromatic rings is an intermediate step in forming the volatile material, generating acetic acid and acetaldehyde, which are decomposed by decarboxylation of acetic acid ( $CH_3COOH \rightarrow CH_4 + CO_2$ ) and decarbonilation of the

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acetaldehyde ( $CH_3CHO -> CH_4 + CO$ ). From the hemicellulose, the resulting product is  $C_2H_4$  and CO from the propanol. In the next zones, there will be sequence in the pyrolysis and oxidation, giving  $CH_4$ ,  $C_2H_4$ , CO and  $CO_2$  as final products.

The pyrolysis of lignin is different in comparison with the hemicellulose and cellulose and at 823 K it produces the following components: coal (55%), gaseous fraction (45%) composed of CO (50%) CH4 (38%), CO2) 10%) and C2H6 (2%). The tar is composed of phenylacethylene, antracene and naphthalene. Table 3 shows the formation of coal in the pyrolysis of several different materials.

Table 3: Coal Formation in the Pyrolysis of Several Different Materials

10 (673K)

Material	Coal (%P)	
Cellulose	14,9	
Popiar (wood)	21,7	
Larch (wood)	26,7	_
Aspen (branches)	37,8	_
Douglas (bark)	47,1	
Klason Lignin	59,0	_

Moisture also has a considerable influence on the particle pyrolysis since it causes an enormous difference in temperature between the particle core and the periphery thereof (400 °K), creating a physical separation between the heating and drying zone and the pyrolysis zone. The dominant influence of moisture is to reduce the flame temperature of the burner, directing the product to coal formation and reducing the rate of pyrolysis. The theoretical flame temperature of the wood combustion is given by:

$$T_a = 1920 - (1.51[TU/(1-TU)] \times 100) - 5.15 X_{exac}$$

wherein Ta (K) is the adiabatic flame temperature, TU is the fraction of the moisture contents, and X exAr is the percentage of air excess. In addition to the

reduction of the adiabatic temperature, there is an increase in the air excess, given by:

$$X_{ext}(\%) = 40[TU/(1-TU)]$$

For TU > 33%, T<sub>a</sub> = 1740°K and for TU = 50%, T<sub>a</sub> = 1560°K and consequently there is a decrease in the volatile content and an increase in the coal content. Finally, one should cite that the ashes reduce the local temperature and catalyze the formation of coal.

Next, the pre-combustion reaction occurs, which represent the cleavage of volatile material into fragments of radicals dominated by reactions of initiation of chains of the type:

$$R-R \rightarrow R + R'$$
 (368kJ/mol)

wherein  $R = C_2H_6$ ,  $CH_3$ , etc. e R''= methylic group.

In wood, the first reaction is most probable due to its lower energy, and an example thereof is given below:

$$C_2H_6 + M \rightarrow 2CH_3 + M$$

$$2CH_3 + 2C_2H_6 \rightarrow 2CH_4 + 2C_2H_5$$

$$M + C_2H_3 \rightarrow H + C_2H_4 + M$$

$$H + C_2H_6 \rightarrow H_2 + C_2H_5$$

wherein M is a heat (ash or vapor)-removing particle or molecule. If R\* contains two or more carbon atoms, the C-C bond is broken preferably instead of the C-H bond. In addition to the reactions of chain initiation, the pre-combustion zone includes reduction reactions with recombinations of radicals R + R' -> R-R', especially if the pre-combustion zone is spatially broad. An example thereof is the recombination of nitrogen forming N<sub>2</sub> instead of NO<sub>2</sub>.

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After the pre-combustion reactions, primary combustion reactions occur: oxygen and fuel mixed in the primary combustion zone results in a number of reactions of free radical, producing  $CO_2$  and  $H_2O$ .

$$RH + O_2 \rightarrow R + HOO$$

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$$CH_3 + O_2 + M \rightarrow CH_3O_2 + M$$

HCO and CO (CH<sub>2</sub>O + (1/2)O<sub>2</sub>  $\rightarrow$  HCO + OH or CH<sub>2</sub>O + O<sub>2</sub>  $\rightarrow$  CO + 2HO) are formed from CH<sub>2</sub>O, and their concentration is maximized at flame temperatures of 1320K, which is the wood combustion temperature.

Finally, the post-combustion reactions occur: the processes of wood combustion occur at low temperature, and reactions of chain end occur in the secondary combustion. The hydroxyl radical (CH<sub>2</sub>O) is of great significance when it is present at high concentrations. The main end reactions are:

$$CO + O_2 \rightarrow CO_2 + O$$

the latter being of lesser importance in this zone. The CO<sub>2</sub> production from CO is controlled by the OH concentration, which is relatively high for low temperature systems (wood). It follows that the chain end is the recombination of H and OH groups aided by heat-removing species (M). The C:H ratio is relatively high for soft wood (1:1.45) and hard wood (1:1.37) compared with mineral coals (1:017). The wood solid pyrolysis produces water, CH<sub>4</sub>, C<sub>2</sub>H<sub>4</sub>, and C<sub>2</sub>H<sub>6</sub>, resulting in a substantial amount of hydrogen in the volatile gases to increase the concentration of hydroxyl radical for a complete and rapid oxidation (greater reactivity). There is no complete expressions in the literature for this system, due to the large number of variables associated to the oxidation of the wood volatiles.

In the combustion of (wood) charcoal, the charcoal obtained from the pyrolysis is porous and contains various free radicals for O<sub>2</sub>attack. In addition, it con-

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tains oxygen and hydrogen, its empirical chemical formula being C6.7H,3,3O. Three mechanisms were proposed for the charcoal oxidation, it being recognized that the combustion rate is limited by the sites of free radicals on its surface. The charcoal oxidation is also limited by the mass transport. The first mechanism is the Boudouard, as the general indicator of charcoal combustion.

This reaction is highly endothemic with the following reaction constants:  $1.1 \times 10^{-2}$  (800°K) and 57.1 (1200°). The CO released is volatile and its combustion is completed in the flame out of the particle. The second mechanism is the chemical adsorption of  $O_2$  directly on the coal. The activation energy of the  $O_2$ adsorption on the porous surface of the coal ranges from 54 kJ/mole to 10 105kJ/mol, respectively, for chemically adsorbed quantities from zero to 2.5 moles of  $O_2$  per gram of coal. The chemical adsorption reactions are:

$$C^* + O_2 \rightarrow C(O)^* \rightarrow C(O)_m \rightarrow CO + CO_2$$

$$C^* + O_2 \rightarrow CO_m \rightarrow CO + CO_2$$

The asterisk indicates an active site of reaction, **m** stands for moveable species, and es stands for stable species. The charcoal active sites can be generated by the mechanism of pyrolysis. The third mechanism of charcoal oxidation involves reactions of hydroxyl radicals in the active sites given by:

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$$2OH + C \rightarrow CO + H_2O$$

$$OH + CO \rightarrow CO + H$$

Hydroxyl radicals are internally generated by homolytic cleavage of the various hydroxylic functional groups existing in the wood or dissociation of the moisture released by the fuel. The moisture influence on the coal oxidation are not well known, as in the case of the pyrolysis of wood. It is speculated that the moisture "deletes" the sites, reducing the rate of coal oxidation. The presence of moisture delays the rate of oxidation of charcoal.

In short, the wood combustion is a multistage process that involves heating and drying, solid state pyrolysis, producing volatile compounds and coal, re-

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actions of gaseous phases (pre-combustion, primary combustion and post-combustion) and combustion of the coal. The various functional groups existing in wood generate a significant number of volatile products from the solid pyrolysis of particles, the various functional groups and the high aliphatic contents increasing the reactivity of wood, contributing to the high proportion of flames in the combustion of the wood with respect to mineral coal. The moisture increases the thermal conductivity, results in greater production of coal in the solid state pyrolysis, increases the concentration of hydroxyl groups for the reactions of gaseous phase and of the coal, and reduces the oxidation rate of the coal, decreasing its temperature and "deleting" the reactive sites.

In view of the complexity and the operational disadvantages presented by the conventional combustion processes, it was desirable to develop a new fuel from biomass that could meet the essential requirements of combustion and overcome the technical drawbacks of the known fuels.

In this regard, various studies have been carried out for the development of new fuels from biomass and some attempts have already presented satisfactory results, as in the case of a cellulignin fuel mentioned in the article "Cellulignin: a new thermoelectric fuel" by Daltro G. Pinatti, Christian A. Vieira, José A. da Cruz and Rosa A. Conte, which relates to a product from generic cellulignin obtained by a process of pre-hydrolysis of biomass without optimized control. However, it was still desired to obtain a fuel that would present even more advantageous results, mainly from the economic point of view and the applications thereof in the main thermoelectric technologies: ovens, boilers, gas turbines and generation of energy by hydrodynamic magnet (MHD).

Therefore, the objective of the present invention it to provide a new cellulignin fuel with catalytic properties that will meet these market requirements with improved combustion characteristics.

#### Summary of the Invention

The present invention relates to a catalytic cellulignin fuel that is composed of cellulose and globulized lignin and that presents a specific surface of about 1.5 - 2.5 m<sup>2</sup>/g, with an average value of 2.0m<sup>2</sup>/g.

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### **Brief Description of the Drawings**

- Figure 1 shows a schematic diagram of the biomass cellular structure.
- -Figure 2 shows the steps of the conventional combustion process of solid fuels.
  - Figures 3a 3e show microphotographs of the structure of a cellulignin according to the present invention, while Figure 4 graphically shows diffratograms of X-rays for wood, cellulose and cellulignin.

Figure 5 shows a graphic of the enthalpy variation for the reactants in a process of catalytic combustion of coal, and Figure 6 shows ratio of the burning time of mineral coal to the particle size. Figures 7a and 7b in turn shows the power irradiated in the combustion of cellulignin according to the present invention.

Figures 8 - 12b illustrate systems and equipment useful for the combustion of the cellulignin fuel now defined.

#### 15 Detailed Description of the Invention

After detailed studies, the inventors achieved a catalytic cellulignin fuel obtained from biomass, which allows a surprising result regarding its combustion. The catalytic cellulign fuel of the invention is prepared by a process of pre-hydrolysis of biomass using a reactor such as described in the Brazilian patent application filed on this same date for "An Apparatus and Process of Pre-Hydrolysis of Biomass". The referred-to pre-hydrolysis may be carried out for any type of biomass, such as wood, sugar-cane bagasse and straw, vegetable residues, barks, grass, organic part of garbage, etc.

The pre-hydrolysis process described in the above-mentioned patent application generically comprises steps of discharging the biomass in a helical feeder, in the device of pre-hydrolysis of biomass, followed by a pressurization operation comprising the following steps: 1) filling the device of pre-hydrolysis of biomass with a pre-heated acidic solution; 2) heating; and 3) pressurization, said process being distinguished by the fact that the pre-hydrolysis is carried out simultaneously with a rotary oscillation of the biomass pre-hydrolysis apparatus, purging of the vapor and controlling the temperature, pressure, acid contents, pre-hydrolysis time,

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and liquid/solid relationship, monitoring the sugar contents until a value of about 10 Bricks is reached by means of a sugar-measuring device. Then, the steps of discharge of the pre-hydrolyzate into a tank through a heat-exchanger, sugar-recovering washing; and discharge of the cellulignin into mechanical washers or carriages to be washed by percolation are carried out.

Again referring to figure 1 and Table 1 presented above, one can see that according to the processes of hydrolysis of biomass the cellulose fibers release is not complete, because the hemicellulose has its highest concentration in the second layer (S2) of its secondary wall. With the pre-hydrolysis process developed by the present inventors, it now has been achieved a product with a specific surface of about 1.5 - 2.52/g, with an average value of 2m2/g, measured by BET (Brunace, Emmett and Teller) and a slush number 100, this meaning that this pre-hydrolysis process reaches the level where partial release of the macrofibrille occurs.

The confirmation of this macrofibrillae release is illustrated in the microphotographs presented in figures 3a - 3e. Figure 3a shows the microstructure of the catalytic celllignin according to the invention after pre-hydrolysis, with an increase of 1000 times (scale of  $10\mu m$ ). Figure 3b shows a cellular wall presenting the middle lamella with an increase of 10.000 times (scale  $1\mu m$ ), while figure 3c shows the cellular wall with an increase of 50.000 times (scale 100nm) and figure 3d shows the cellular wall with an increase of 100.000 (scale of  $10\mu m$ ). Figure 3e shows the microstructure of a second sample where it is possible to observe the lignin globulization.

The combination of an open structure, while maintaining the crystalline characteristics of cellulose demonstrated by X-rays diffraction, as can be seen in figure 4, enables one to achieve the following characteristics of the cellulignin fuel:

1 - due to the maintenance of the cellulose crystalline characteristics, it is possible to effect the grinding of the cellulignin according to the present invention down to below 200µm by using hammer mills without the need for intermediate sieving and with a low energy consumption (about 12kWh/t). Due to this characteristic, the new fuel is called "catalytic" lignin.

2 - Easy drying of the water in rotary dryers, ovens or cyclones: the cellulignin according to the invention, which has particle size below 200μm, presents a completely open structure which permits it to be dried at 500ppm of moisture and at low temperature, that is to say, at 125° C (temperature of chimney gas).

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The water contained in biomass is one of the worst characteristics for combustion, and the drying achieved for the cellulignin of the invention allows the obtention of a value of 18<sup>A</sup> 20MJ/kg for the combustion heat, which is the double of the combustion heat of biomass with normal moisture of 45%.

Therefore, one of the great technical advantages obtained by the present invention is that the catalytic cellulignin may be externally dried with the heat of the chimney gas and subsequently burned in dry form. This option is unfeasible for raw wood.

- 3 When in the powder form, the cellulignin density is of 600kg/m3 in the so-called accommodated form, and 450kg/m3 in the non-accommodated form. This represents an average energetic density of 20MJ/kgx500kg/m3 = 104MJ/m3, compared with the energetic density of 40MJ/kgx800kg/m3 = 3.2x10<sup>4</sup>MJ/m3 for fuel oils, which means that the tanking and handling of the catalytic cellulignin fuel are only three times as high as those of fuel oils, and it is drastically easier than the handling of raw biomasses (wood and vegetable residues), which require large volumes and huge equipment.
- 4 The dosage of the cellulignin of the invention in combustion apparatus is made, for instance, by means of helical dosing device or rotary valves and the feeding of air such as drag-gas air in the proportion of air:cellulignin of about 3.28:1 by weight and 1261.6:1 by volume. This imparts to the cellulignin a characteristic equal to that of the gases or liquids in the operations of dosing and feeding, providing a drastically easier operation than the conventional dosing and feeding of solid fuels, especially biomasses.
- 5 The microstructures pictures show the disclosure of the microfibrillae in a dimension of 50nm. This technique establishes the correlation between the process (hemicellulose digestion) and the product (open structure with medium specific surface). It constitutes one of the main new characteristics of the product, as well as the technology of controlling the pre-hydrolysis process in the production of the catalytic cellulignin fuel.
- 30 6 Table 4a illustrates the physical characteristics of the Micropores (Active Sites) and table 4b presents the distribution of the Meso and Macropores. The former was determined by BET - Adsorption of N2 and the latter was determined by

Hg porosimetry. The total specific area measured by BET is about 2.20m2/g, and the specific area of the macro and meso pores were the larger portion of the total area. The calculation thereof from the average radius of the pore measured by Hg porosimetry results in 1.80m2/g, admitting a cylindrical symmetry of the pore (I = 2r). This conclusion is coherent with the low micropores volume (1.1x10<sup>-3</sup>cm3/g) measured by BET. The distribution of the macro and meso pores has its maximum value ranging from 1 to 5µm (1000 - 5000nm), this size coinciding with the voids of the of the cells photographed by MEV (figures 3a, 3b, and 3e). The data of table 4 and the microstructures of MEV permit the complete characterization of the catalytic cellulignin fuel according to the present invention. The micropores are measured by the iodine number equal to 100; in the case of the catalytic cellulignin still there is no instrumentation that enables one to appraise the of the micropores (2nm) contribution in the combustion.

Table 4a: Physical characterization of the Micropores

(Active Sites -  $\phi$  < 2.0nm)

Samples	Crystalline	Specific	Micropore	Micropore
	density <sup>(1)</sup> .	area <sup>(2)</sup>	Radius <sup>(2)</sup>	volume <sup>(2)</sup>
	(g/cm³)	(m²/g)	(nm)	(x10 <sup>-3</sup> cm3/g)
1- Wood	1,284	0,459	0,948	0,217
2 - Cellulignin without			•	
grinding - pre-hydrolysis				
time	1,331	0,756	0,980	0,371
2a - 0,5h (oscilation)	1,337	1,463	0,905	0,662
2b - 1,0h (oscilation)	1,334	1,342	0,970	0,651
2c - 1,0h (static)	1.351	2,249	0,964	1,080
2d - 2.0h (oscilation)				
3-Griding effect			<u> </u>	
3a-cellulignin without	1,252	2,483	1,197	1,496
grinding	1,353	2,758	0,997	1,375
3b- 297µm<¢<354µm	1,368	2,013	1,135	1,143
3c- 177µm<ф<210µm	1,375	2,114	1,032	1,090
3d- 125µm<φ<149µm	1,372	1,915	0,962	0,921
3e- 88µm<ф<105µm	1,346	3,179	0,914	1,454

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3f- φ<74μm	T				
4- Wood and carbonized			•		
Cellulignin					
4a- carbonized wood	1,314	0,965	1,024	0,494	
4b- cellulignin de 0,5h	1,292	2,474	1,014	1,254	
4c- cellulignin de 1,0h	1,327	1,452	1,002	0,727	
4d- cellulignin de 2,0h	1,371	1,932	1,009	0.974	•
4e- double carbonization	1,421	2,497	1,000	1,248	

<sup>(1)</sup> Picnometry of Helium; Equip. used: Ultrapicnometer - Model: 1000 from Quantachrome - Version: 1.62

<sup>(2)</sup> BET - Adsorption of N2; Equip. used: Adsorptometer - Model: Nova from Quantachrome - Version 3.70

Table 4b: Distribution of Meso (2nm < 0 < 50 nm) and Macro (0 > 50 nm) pores ( $cm^3/g$ )

Cylindrical Geometri of the Pore ( r = 21 ) (\$\scrt{SN}\rightarrow{\circ}\rightarrow		2,668	2,080 1,765	2,004	1,553	1739	3,676	S = Surface of the pore V = Volume of the pore r = Radius of the pore I = Length of the pore
	Total	0,421	0,232	0,212	0,229	0,218	0,830	
	2x10' <d,<5x10'< td=""><td>0.056</td><td>0,046</td><td>0,035</td><td>0.049</td><td>0,042</td><td>0,530</td><td></td></d,<5x10'<>	0.056	0,046	0,035	0.049	0,042	0,530	
(nm)	10'xD <sub>6</sub> <2x10'	0,038	0,052	0,062	0,058	0,081	0,163	
Porosimetry of Mercury D <sub>p.</sub> Pore Diameter (nm)	100 <d,<1000< td=""><td>0,084</td><td>0,095</td><td>0.094</td><td>080'0</td><td>160,0</td><td>0,108</td><td></td></d,<1000<>	0,084	0,095	0.094	080'0	160,0	0,108	
	10 <d,<100< td=""><td>0,076</td><td>0,033</td><td>0,018</td><td>0,025</td><td>0,026</td><td>0,023</td><td></td></d,<100<>	0,076	0,033	0,018	0,025	0,026	0,023	
	D,<10	0,016 0,004	800.0 800.0	0,003	0,007	600'0	800'0	
	Average radius (nm)	631,2 1025,2	693,0 967,2	845,8	1180,6	1003,2	1716,4	
	Samples	3s. cellulignin without grinding 0 > 2mm 0 > 354 µm	3b- 297µm<0<354µm 210µm<0<250µm	3c- 177µm<0<210µm 149µm<0<177µm	3d- 125µm<0<149µm 105µm<0<125µm	36- 88µm<0<105µm 74µm<0<88µm	36- 0<74Jim	

7 - The major application of the cellulignin of the present invention is as a fuel for boilers, gas turbine and for the generation of energy by magnet hydrodynamics (MHD). However, apart from the usesas a fuel, there are several other applications in the following areas: a volume component for animals food, pyrolysis for the production of oils and activated coal, production of carbon black (incomplete combustion), production of methanol, cellulignin resinates (agglomerates, MDF - Medium Density Fiber), substrate for semisolid fermentation (fungi, bacteria and enzymes), etc.

Even though the precise chemical formula of the cellulignin according to the invention may vary, its empirical chemical formula is presented in Table 5, in comparison with the empirical formulas of wood, biomass components, mineral coal and fuel oils, these data providing a good reference for the understanding of the improved effects achieved by the fuel developed now.

Table 5: Chemical formulas of the several fuels

15	Fuel	Material	Carbon	Ashes	Empirical formula
	(moisture)	Volatile (%)	fixed (%)	(%)	approximate
	1. Soft wood (46%):				
	Douglas fir	86,2	13,7	0,1	C4.4H6.3O2.5NT -
	Pitch pine	•	•	-	C4.9H7,2O2.0Nv
20	Hemlock	84,8	15,0	0,2	C42H64O28Nv
•	2. Hard wood (32%):				•
	Poplar	-	•	-	C <sub>4,3</sub> H <sub>6,3</sub> O <sub>2,6</sub> N <sub>6</sub>
	White ash	• • ••	•	-	C4,1H7,0O2,7N#
	3. Barks:				•••
25	• Oak	-	•	•	C3.3H5.4O3.1Na
	• Pine	•	-	•	C45H56O24Nv
	4. Wood				
	• Dry (17%)	-	•	• .	C4.4H6.0
					O <sub>2.4</sub> N <sub>0.02</sub> (H <sub>2</sub> O) <sub>1,1</sub>
30	<ul> <li>Humid (50%)</li> </ul>	-	•	.•	C <sub>4,4</sub> H <sub>4,0</sub>
					O <sub>2.4</sub> N <sub>0.002</sub> (H <sub>2</sub> O) <sub>5.6</sub>

	fuel	Material	Carbon	Ashes	Empirical formula
	(moisture)	Volatile (%)	fixed (%)	(%)	approximate
	5. Components of				
5	biomass:				
	• Cellulose				(C <sub>6</sub> H <sub>10</sub> O <sub>5</sub> ) <sub>n</sub>
	Hemicellulose				$(C_5H_{10}O_5)_n$
	• Lignin	•			(C <sub>10</sub> H <sub>7</sub> O <sub>4</sub> ) <sub>n</sub>
	Catalytic cellulignii	n			$C_{5,5}H_{4,2}O_{1,8}N_{v}$
10	Cellulose coal		-		C <sub>6.7</sub> H <sub>3.3</sub> O <sub>1.0</sub> N <sub>4</sub>
	6. Tar.				C <sub>4,7</sub> H <sub>5,8</sub> O <sub>3,0</sub> N <sub>tr</sub>
	7. Mineral coals:			•	
	<ul> <li>Lignite (37%)</li> </ul>	•	•	•	•
	<ul> <li>Subbitumenous</li> </ul>				
15	A(14%)	•	•	•	-
	B(25%)	40,7	54,4	4,9	$C_{6,0}H_{4,8}O_{1,0}N_{\pi}$
	C(31%)	•	-	•	•
	<ul> <li>Bitumenous</li> </ul>			•	
	Low volatile	17,7	71,9	10,4	C <sub>6,7</sub> H <sub>4,3</sub> O <sub>0,14</sub> N <sub>0,11</sub>
20	Medium volatile	•	•	•	•
	High volatile	6,4	81,4	12,2	$C_{6,8}H_{2,3}O_{0,12}N_{0,09}$
	Antracitic	6.4	81,4	12,2	C <sub>6.8</sub> H <sub>2.3</sub> O <sub>0,12</sub> N <sub>0.06</sub>
	8. Oils (APF - A1)	•	• '	•	C7.3H11.1O0.09N0.02

As can be seen, biomasses have low carbon contents (4.3 moles per formula-gram), middle hydrogen contents (6.5 moles per formula-gram), and high oxygen contents (6.5 moles per formula-gram). Mineral coals have high carbon contents (6.5 moles per formula-gram), low hydrogen contents (4.3 moles per formula-gram), and low oxygen contents (0.15 moles per formula-gram). The catalytic cellulignin according to the invention is in an intermediate position with carbon (5.5) and hydrogen (4.2) contents tending to mineral coal, but with intermediate oxygen contents (1.8 moles per formula-gram). In fact, the catalytic cellulignin comes close to lignite coal being obtained, however, in 20 minutes of pre-hydrolysis, while lignite coal took millions of years to be formed.

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Another great advantage of the cellulignin fuel developed now is its very low ashes contents, thus meeting, for instance, the requirements of clean fuel for gas turbine (Na + < 5 ppm) when processed in pre-hydrolysis with deionized water. This is due to the pre-hydrolysis process efficiency that solubilizes K in the form of water-soluble  $K_2SO_4$ , which is later leached in the washing step. All impurities contained in the wood are reduced and even those of higher contents, such as Ca, Mg, al, and Si present in eucalyptus wood, for example, do not cause hot corrosion on the superalloys of the gas turbines. The cycloning of the combustion gases from the fuel of the invention proved to be highly efficient in reducing the ashes contents at the level required for gas turbines (total particulate < 200ppm and particulate with a diameter >  $5\mu m$  being in a proportion lower than 8ppm).

A few points should also be stressed with respect to the improved characteristics of the cellulignin fuel of the present invention, which bring expressive advantages for combustion processes, when compared to conventional fuels.

As already mentioned before, in the solid pyrlysis zone in a combustion process, high temperatures favor the production of volatile compounds, and low temperatures favor the production of coal. As already indicated by table 2 above, the products resulting from the cellulose and xylan pyrolysis result in high tar contents, which causes a secondary combustion close to the oils for wood. However, there is no xylan in the catalytic cellullignin according to the present invention, which leads to lower coal contents in this zone. It is further pointed out that the globulization of lignin in the production process of catalytic cellulignin fuel of the invention favors the formation of volatiles and decreases the coal contents. In addition, and considering the influence of moisture on the particle pyrolysis, it follows that the catalytic cellulignin fuel maximizes the combustion temperature, increases the volatile contents and decreases the formation of coal contents since provides the possibility of a burning without moisture and with low ashes contents.

Other technical advantages obtained according to the invention may be clearly observed during the pre-combustion reactions and in the primary combustion reactions, as well as in the post-combustion reactions of the cellulignin fuel.

In the pre-combustion step, it is observed that, in the case of the catalytic cellulignin, there is a decrease in the ash contents, the water contents and

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xylans are non-existent, and these aspects favor CH<sub>4</sub> formation (a product from the decomposition of R\*-cellulose) instead of C<sub>2</sub>H<sub>6</sub> (product from the decomposition of hemicellulose, non-existent in cellulignin). During the primary combustion, the combustion of cellulignin takes place at higher temperatures, like the combustion of CH<sub>4</sub> resulting from the decarboxilation of the acetic acid and decarbonilation of the aceticaldehyde resulting from the opening of the rings. This explains why, in practice, the catalytic cellulignin has a combustion similar to that of natural gas and of volatile liquid fuels. Finally, during the post-combustion step the ratio C:H is of 1:0.76 for the case of the catalytic cellulignin, that is to say, it is closer to the mineral coals than to wood. The average oxygen contents, however, favor the formation of CH<sub>4</sub>, CO<sub>2</sub> and CO, reinforcing the explanation for the high reactivity of the catalytic cellulignin.

In order to enable a better understanding of the similarity of the features of combustion of the catalytic cellulignin of the present invention as compared with those of the mineral coal, a modern theory of the combustion of porous particles (Essenhigh) is given below in view of its significance for the invention of the combustion of cellulignin.

The mass loss rate:  $m = m(a,\sigma)$  wherein m = mass of the spherical particle, a = particle radius, d = 2a = particle diameter,  $\sigma = particle$  density and m = (4/3)  $\pi a^3 \sigma$ .

$$\frac{dm}{dt} = \frac{\partial m}{\partial a} \frac{da}{dt} + \frac{\partial m}{\partial \sigma} \frac{d\sigma}{dt}$$

$$\frac{dm}{dt} = 4\pi a^2 \sigma \frac{da}{dt} + \frac{4}{3}\pi a^3 \frac{d\sigma}{dt}$$

$$R_s = \frac{dm/dt}{4\pi a^2} = \sigma \frac{da}{dt} + \frac{a}{3} \frac{d\sigma}{dt} = R_e + R_i = R_e \left[1 + \frac{R_i}{R_e}\right]$$

$$\frac{R_i}{R_e} = \frac{a}{3\sigma} \frac{d\sigma}{da} = \frac{1}{3} \frac{d(\ln \sigma)}{d(\ln a)}$$

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 $R_s$  = mass loss rate by the external surface of the particle (g/cm²s) e R<sub>s</sub> is the mass loss rate by the internal surface. The above equation is an inexact differential equation impossible of being integrated due to the lack of a relationship between  $\sigma$  and the a (integration way).

Essenhigh (1988) proposed the utilization of the equation of Thiele (1939) of catalysis as a way of integration of  $R_{\rm s}$ 

$$\frac{\sigma}{\sigma_0} = \left(\frac{d}{d_0}\right)^{\alpha} = \left(\frac{a}{a_0}\right)^{\alpha} :: \alpha = \frac{d(\ln \sigma)}{d(\ln a)}$$

wherein  $\alpha=0$  stands for density,  $\sigma$  constant with combustion by the external surface and  $\alpha\to\infty$  stands for constant diameter with combustion over the internal surface (This concept is similar to the catalysis over the external surface or over the internal surface).

Calculating the R/R<sub>e</sub> relationship it follows that:

$$\frac{R_t}{R_s} = \frac{R_t}{R_{so}} \frac{R_{ion}}{R_s} = \eta \frac{R_{ion}}{R_s}$$

wherein  $R_m$  is the maximum rate of internal loss and  $\eta = R/R_m$  is the Thiele effectiveness factor (0 <  $\eta$  < 1) representing the relationship between the real internal loss and the maximum possible internal loss (For large particles or particles of low porosity, the internal mass loss is negligible and  $\eta \rightarrow 0$  while for small particles and high density the internal loss of mass is maximum and  $\eta = 1$ ).

Defining  $S_v$  as the internal surface area per volume unit  $V_p$  ((cm²/cm³) = 1/cm) and  $S_p$  as the external surface area of the particle, it follows that the relationship  $R_m/R_v$  is proportional to the relation of the internal and external areas in:

$$\frac{R_{im}}{R_e} = \frac{V_p S_v}{S_p} = \frac{\frac{4}{3}\pi\alpha^3 S_v}{4\pi\alpha^2} = \frac{aS_v}{3}$$

$$\frac{R_i}{R_e} = \frac{a}{3} S_v \eta = \frac{1}{3} \frac{d(\ln \sigma)}{d(\ln a)} = \frac{\alpha}{3}$$

$$\alpha = aS_v \eta$$

For mineral coals,  $\alpha$  ranges from zero to 3, exceptionally reaching the value of 6. For the catalytic cellulignin fuel, we have  $S_v = \sigma S_g$ , wherein  $\tilde{S}_g$  is the in-

ternal surface per unit of mass, the following values resulting for a particle of 200  $\mu m$ :

S.	m²/g	0,01	0,1	0,2	0,3	0,4	0.5	1,0	10,0
	m²/kg	10	10²	2×10²	3×10 <sup>2</sup>	4×10 <sup>2</sup>	5×10 <sup>2</sup>	103	104
α =	aσS <sub>e</sub> η	1	10	20	30	40	50	100	1000
	)= (d/d <sub>0</sub> ) <sub>a</sub> /d <sub>0</sub> )=0.9	0.9	0,349	0.122	0.042	0,015	0,005	2,7× 10 <sup>-5</sup>	1,7× 10 <sup>-46</sup>

This means that for a specific surface larger than 0,4m2/g ( $\alpha$  = 40), the catalytic cellulignin fuel burns mainly from the internal surface, maintaining the particle diameter approximately constant and varying its density (burning of a fractal - 1° zone), characterizing the new invention as a large-scale, completely catalytic, fuel obtained from the pre-hydrolysis of biomass available in nature. Tests of specific surface (BET, porosimetry of mercury and MEV) indicate an average value of 2.0m2/g, resulting in  $\alpha$  = 200. The particles of liquid fuel burn from the external surface ( $\alpha$  = 0 - 3° zone), and the particles of mineral coal have partial internal combustion (0 = or <  $\alpha$  = or < 3 - 2° zone).

- For the case of mineral coal,  $\alpha$  = Sv/ $\!\gamma$  , wherein  $\gamma$  is the Thyele parameter given by:

$$\lambda = (S_{\star} \overline{\kappa} / \rho D_{\epsilon})^{1/2}; \alpha = (\rho D_{\epsilon} S_{\star} / \overline{\kappa})^{1/2}$$

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wherein k = constant of the reaction rate,  $\rho$  = reactive gas density and De = coefficient of internal diffusion. For the catalytic cellulignin there is no need for independent determination of these parameters, because they combine, resulting in a relatively high value of  $\alpha$  ( $\alpha$  = or> 100).

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- In the catalytic combustion, the oxygen does the direct attack on the carbon atom as a two-stage reaction (adsorpotion-desorption), illustrated in figure 5. Oxygen is adsorbed and desorbed, forming CO<sub>2</sub> or CO, which is then deadsorbed.

The components and products of the reaction are C, O<sub>2</sub>, CO<sub>2</sub>, H<sub>2</sub>O, H<sub>2</sub>, and CO, ac-

$$2C_{f} + O_{2} \xrightarrow{h} 2C(O)$$

$$C_{f} + CO_{2} \xrightarrow{h} C(O) + CO$$

$$C_{f} + H_{2}O \xrightarrow{h} C(O) + H_{2}$$

$$2C_{f} + H_{2} \xrightarrow{h} 2C(H)$$

$$C(O) \xrightarrow{h} CO + C_{f}$$

$$2C(O) \xrightarrow{h} CO_{2} + C_{f}$$

cording to the following reactions:

wherein Cf indicates a free site, C(O) stands for a chemically adsorbed oxygen atom and ki are reaction constants. The volatiles (CO, H<sub>2</sub>) produced by the catalytic combustion complete their combustion outside the particle with a very short combustion time (3 ms). The determined combustion time is that of the adsorption-deadsorption process, being equal to or shorter than 20 ms (0.02s) for the catalytic cellulignin.

The burning time for mineral coal, liquids (oils) and for catalytic cellu10 lignin fuel measured in the form of isolated particle and in the form of powder cloud
is illustrated in figure 6 and the formulas utilized in the corresponding calculations
are presented below.

## **Attachment I: Combustion Times**

1a - Coal Cumbustion

15 Burning time

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i) at constant density:

$$t_b = \frac{\rho_0 R T_m}{96 \phi D p_g} d_0^2$$

ii) at constant diameter

$$t_b = \frac{\rho_0 R T_m}{144 \phi D p_g} d_0^2$$

wherein:

 $\rho_0$  = initial density of the particle  $\cong 1000 \text{kg/m}^3$ 

R = universal constant of the gases = 0,8106m3atm/(kmolK)

T<sub>m</sub> = average temperature = 1600K

D = diffusion coefficient = 3,49x10<sup>-4</sup> m<sup>2</sup>/s

P<sub>a</sub> = partial oxygen pressure = 0,2atm

 $\phi$  = order of reaction = 2

do = initial particle diameter (m)

1b - Combustion of Liquids

10 Burning time

$$t_b = \frac{d_0^2}{\lambda}$$

wherein:

do = initial diameter

 $\lambda$  = evaporation rate = 10±2)x10<sup>-3</sup>cm<sup>2</sup>/s for hydrocarbons burning in air.

In the first form, the burning time is shorter than that of mineral coal because it is a much more reactive fuel. In the form of a powder "cloud", there is a decrease in the thermal losses due to the energy transmission by radiation among the particles, decreasing the burning time for values similar to those of the volatile liquids. One way of analyzing this question is by means of the Krishna and Berlad's energy balance for ignition of powder cloud of mineral coal.

$$(const)T_i^{\beta-1} = \frac{\lambda_0/a}{1 + R^2D/a^2\sigma}$$

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wherein the first term is the energy generation rate, a is the radius of the particle, R is the radius of the cloud,  $\rho$  is the particle density, D is the density of the cloud,  $\lambda_0$  is the air thermal conductivity and  $\beta$  is an empirical coefficient. If  $R^2D/a^2\sigma$  << 1 it follows that  $aT_{\beta}^{-1}=(const.)$  and if  $R^2D/a^2\sigma>>1$ , then  $T_{\beta}^{-1}=(const)a$ . The latter is in accordance with the world experience that recommends grinding the mineral coal at temperatures not higher than 70°C to avoid incineration of the powder cloud in the mills. For catalytic cellulignin fuel injection, we have R=0.1m,  $a=100\times10^{6}m$ ,  $\sigma=500~kg/m^3$ ,  $D=0.4kg/m^3$  resulting in  $R^2D/a^2\sigma=800>>1$ . The smaller the particle size, the lower the ignition temperature of the powder cloud. For mineral coal, the theoretical ignition temperature of the cloud is 300 at 500°C and for catalytic cellulignin, the ignition temperature is on the order of 350°C (pyrolysis temperature). The presence of oxygen in the molecule of the catalytic cellulignin fuel favors the similarity of its combustion process to that of mineral coal (however, with higher reactivity and higher ignition temperature) with respect to the combustion of wood, which is of five steps and seriously limited by the presence of water.

In order to establish the combustion characteristics, catalytic cellulignin particles of different diameters were burned by means of LASER ray ignition and determination of irradiation intensity with photodiodes. The results are shown in figures 7a and 7b, where one can see two regimes, namely: 1) above 250 $\mu$ m the combustion is of the conventional type (limited by the transport of mass inwards and outside the particle) and 2) below 25°  $\mu$ m the combustion is not limited by mass flow (process of adsorption of  $O_2$  - deadsorption of  $O_3$ ). The two regimes adjust to Thiele's catalytic combustion. Attention is drawn to the importance of maintaining the crystalline characteristic of the cellulose in the pre-hydrolysis process to render the grinding of cellulignin particles smaller than 250 $\mu$ m inexpensive.

a) Conventional combustion ( $\phi > 250 \mu m$ ): the catalytic cellulignin is dried outside the combustion equipment and the drying zone is non-existent. The heating is rapid, the generation of volatiles is maximized while coal generation is minimized. The catalytic cellulignin does not contain xilan, its solid pyrolysis predominating, that is to say, opening of the ring with production of acetic acid, acetaldehyde and coal by decarbonilation of the acetic acid and decarboxylation of the acetaldehyde in the formation of CH<sub>4</sub>, CO<sub>2</sub> and CO. The zones of volatiles primary and secondary combustion are the same as described before.

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b) Catalytic combustion (φ < 250μm): The pre-hydrolysis displaces the biomass in the direction of the combustion of mineral coal. The main characteristic is that combustion is more limited by the mechanism of the oxygen transport into the catalytic cellulignin and of CO therefrom due to the particle microstructure. In this way, there physical (O<sub>2</sub>) and chemical (O) adsorption in active sites and Boudouard's reaction is favored. Reactions of hydroxylic groups cause rapid reactions in the heating and solid pyrolysis zones. The catalytic combustion occurs in the average internal surface (2.0m2/g), the contribution of the external surface (0.1m2/g) of the particle being secondary. The framework of the catalytic cellulignin is that of a fractal that burns while maintaining the diameter of the particle approximately constant and decreasing the particle density. When the wall of the fractal thickness reaches a critical size, a collapse of the particle (sublimation) takes place. Therefore, the process eliminates the formation of residual coal, resulting in complete combustion.

The combustion equipment usable for the catalytic cellulignin of the present invention will depend upon the type of specific combustion to be employed. In this regard, the main methods of biomass combustion are: combustion in pile, thrower-spreader, suspension, and fluidized bed, the thrower-spreader combustor is the most prominent from the industrial point of view. The characteristic of the first two is the complete physical separation of the five combustion zones. In the combustion by suspension of dry biomass particle ( $\phi$  < 2mm, TU < 15%), all "zones" take place in the middle of the air, in a sequential way. The suspension burning is the closest to the burning of liquid fuels. This is the case of the cellulignin proposed now, which comes close to the combustion of gases and liquids due to its catalytic combustion.

The combustion in fluidized bed maintains the fuel in a bed with sand or lime suspended by air. All the reaction zones take place in the same place (not separable physically). The combustion efficiency is low due to the excess air (100 - 140%) necessary to maintain the fluidized bed, and the temperature is kept below the ashes melting point in order not to cause the bed to collapse. In the case of the catalytic cellulignin of the invention, the suspension combustion may be carried out with stoichiometric air and without limitation of temperature, since it has a very low

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ash content. The three main parameters in the combustion are useful heat, thermal efficiency and combustion temperature.

$$Hv = CCS - PT; \eta = [1 - (PT/CCS)]x 100$$

wherein CCS is the upper calorific capacity and PT are the thermal chimney losses, ashes (including not-burnt carbon), radiation and others. The chimney losses are given by:

$$PT = \sum_{i=1}^{n} m_i (C \rho_i \Delta T) + m_{H,O} \lambda_{H,O}$$

wherein mi is the moles of the chimney gases (CO<sub>2</sub>, O<sub>2</sub>, N<sub>2</sub>, H<sub>2</sub>O), Cpi is the calorific capacity of each species,  $\Delta T$  is the difference in temperature between the chimney and the environment, m<sub>H20</sub> is the number of moles of water and  $\lambda_{H20}$  is the molar water vaporization value.

The losses by radiation are of about 4% and other losses (ash, not-burnt carbon) are about 2%. The combustion efficiency of a wood with 50% moisture is 68%; with 17% moisture, it is 79%, and that of the catalytic cellulignin is 85% (close to the values of the mineral coal) due to the absence of moisture, ash and excess air. The catalytic cellulignin fuel of the invention permits the achievement of temperatures close to the adiabatic one (1920 K), although the temperatures of the vapor-generating tubes of the boilers are limited to 840K.

The heat release rates for the different combustion methods are given by  $I = h \, dW/dt$ , wherein I is the flame intensity, dW/dt is the change in weight in function of the time, and h is the combustion heat. Table 6 shows several rates for the different combustion methods:

Table 6: Heat release rates for different combustion methods.

Wood	Mineral coal
8,5GJ/m²h	
3,5GJ/m²h	_
10,4GJ/m²h	8,8GJ/m²h
	8,5GJ/m²h

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Suspension	550GJ/m³h	
Fluid bed	470GJ/m³h	

The reactivity of the catalytic cellulignin is slightly higher than that of biomass (absence of water, larger specific surface) and the combustion heat is the double, leading to a heat release rate twice as high as that of wood. For example, 9kg/h of catalytic cellulignin with combustion heat of 20MJ/jg burn in suspension in a volume of  $\phi$  = 2cm and L = 50cm, that is,  $(9\times20/(\pi\times(0.01)^2\times0.5) = 1.146\text{GJ/m}^3\text{h}$ .

The examples of equipment given below will better illustrate the present invention in a better way. However, the data and procedures illustrated merely refer to a few embodiments of the present invention and should not be taken as being limitative of the scope of the invention.

The complete characterization of the catalytic cellulignin fuel involves elements of the cellulignin as starting material, of the combustion specific characteristics and of the fuel handling and controlling equipments.

Figure 8 illustrates a feeding system composed of a cellulignin tank (8.1), a rotary valve or helical feeder for dosing the cellulignin feed (8.5 and figures 9 and 10), feeding line of the air/cellulignin two-phase fluid (rate 3.28:1 by weight) (8.6) and applications in boilers and ovens (pressure close to the atmospheric one, T = 1900° C), in gas turbines (pressure of 7 - 14 atm, T = 600 - 1100° C). The cellulignin tank may be either stationary (preferably in vertical cylindrical form), or moveable (installed in carriage similar to the tanks for carrying animal food or cement). Due to the tendency of cellulignin to settle, the tanks are preferably provided with a conic or plane bottom and with powder handlers of the rotary-shovel type (8.2, 8.3, 8.4), helical feeders or a bottom with moveable compressed-air lining. At the exit of the rotary valve or helical feeder for dosing the cellulignin, drag air is injected for 25 two-phase flow at the ratio of 3.28:1. The two-phase flow may be made of metallic, plastic pipes or hoses, the air/cellulignin mixture behaving as if it were a gas or a liquid. Under low pressure, the energetic density of the air/cellulignin mixture is of 7.14MJ/m3, while that of natural gas is 32.9MJ/m3 and that of the fuel oils is 28.0MJ/m3, permitting still compact, simple installations and significant lengths of the piping, in order to meet the layouts of the factories, thermoelectric power stations, etc.

The helical feeder shown in figure 9 is composed of a body (9.1), bushing (9.2), helical feeder (9.3), powder retainer (9.4), bearings (9.5), flanges 5 (9.6), driving pulley (9.7) and air injection for two-phase flow (9.8). The dosage of cellulignin is carried out by turning the helical feeder and varying its diameter and, in general, it is utilized for low capacities (<150 kg/h). The elimination of the influence of pressure difference between the cellulignin tank and the drag gas in dosing the powder carried by the helical feeder is carried out by means of the impedance of the length of the helical feeder between the tank body and the drag air of the two-phase flow. The rotary valves illustrated in figure 10 are available on the market for capacities higher than 150 kg/h and comprise a body (10.1), shovels (10.2), driving shaft (10.3), inspection window (10.4) and possibly cooling (10.5). The dosage is made by means of rotation, the diameter and the length of the valves.

### Combustors

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The direct use of combustors in boilers and ovens is possible because of the low content of the cellulignin ashes (<0.2%) and the resources already existing in this equipment for removing residual ashes. For applications in gas turbines, the following measures are necessary: a) combustion chamber with injection of primary air (stoichiometric combustion) and secondary air (drag of the ashes from the combustion chamber to the cyclone and cooling of the combustion gases down to the working temperature of the turbine); b) gas-cleaning cyclone (removal of the particulate); and c) possible ceramic filter for high temperature turbines (1100° C monocrystalline superalloys), and these filters are indispensable to polycrystalline superalloys or with directional solidification. The specifications of Na + K < 5ppm, in the catalytic cellulignin fuel with total particulate contents of 200ppm, with diameter > 5µm lesser than 8ppm in the combustion gases, have been achieved, without the need for ceramic filters.

#### **Axial Combustor**

30 Figure 11 shows an example of an axial combustor to characterize the combustion of the catalytic cellulignin. The ignition may be carried out in several

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ways, such as by microblowtorches of GLP, natural gas, etc., electric arc, electric resistance or hot gas tube. The fact that it is easy, automation and low cost favor the ignition with blowtorches of GLP, natural gas (consumption of 0.022 kg of GLP/kg of cellulignin, representing 5% of the calorific capacity of the combustor). Two factors related to catalytic cellulignin ignition are pointed out: first, the need for it to be heated up to the pyrolysis temperature (350° C); second, the operational security of the catalytic cellulignin with respect to the combustible gases and liquids that ignites at room temperature. The practical applications may be made with any type of combustor (axial, swirler, cyclonic, etc.)

The axial combustor is composed of a mounting plate (11.1) with or without cooling, cellulignin injector (11.2), stoichimetric-combustion-air injector (11.3), fixture of the ignition blowtorches (11.4) with or without cooling, ignition blowtorch of GLP, natural gas, etc. (11.5), window with view-finder (11.6). Ignition blowtorches are as small as available on the market, because the catalytic characteristics of cellulignin enable their instantaneous ignition and propagation for the two-phase air/cellulignin flow. The power of the ignition blowtorch is on the order of 5% of the power for low capacity (50kW) combustors and tends to negligible percentages for high capacity combustors. For the two-phase flow with velocity of 8.5m/s and a diameter  $\phi$  = 16.5 mm, the ignition spreads at a length of 100 mm, giving an ignition time of 0.012s = 12ms. The combustion is complete at a length of 0.7m, giving a residence time of 1/(8.5/2) = 0.16s = 160ms (one has utilized the average velocity of 8.5/2 = 4.25m/s, since the injection velocity in the beginning of the flame is of 8.5m/s and the velocity at the end of the flame is virtually nil). The resistance-time/ignition-time relationship is on the order of ten times. The ignition times of the catalytic cellulignin tend to the ignition times of gases, which are on the order of 3ms.

In general, mineral coal and liquid fuels generate a very long flame length, due to the longer burning times (see figure 6), thus requiring combustors of the axial-swirler type for reducing the flame length. The catalytic characteristic of cellulignin allows one to use axial combustors with relatively short flame lengths. The extinguishing of the ignition blowtorch results in extinguishing the flame of the catalytic cellulignin, due to the need for it to be pyroliyzed at 35° C, imparting to the catalytic cellulignin complete security in its handling (non-incendiary and non-

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explosive fuel) The catalytic cellulignin does not contain hemicellulose, which is responsible for the incendiary characteristic of biomasses in the form of straws (pyrolysis temperature = 200° C), as well as it does not pyrolyze at low temperature, and so does not have the incendiary characteristics of the gases and liquid fuels (low flash point). On the other hand, above 350° C, its combustion is catalytic with ignition times close to that of gases.

## Gas Turbines

For applications of cellulignin combustors in gas turbines, two additional steps are required, namely: cooling of the gases and a cyclone for reducing particulates. Figures 12a and 12b show the cellulignin combustor, cycloning and particulate collector with horizontal or vertical assembly. It is composed of combustor (12.1), combustion chamber (12.2), inlet of cooling air (12.3), chamber of cooling air (12.4), homogenization sector (12.5), cyclone (12.6), particulate collector (12.7), and duct of connection with the turbine (12.8). In the vertical position, an ash collector (12.9) is added before the combustion gases are directed to the cyclone for collection of the molten ashes during the stoichiometric combustion.

The combustor illustrated is manufactured from stainless steel, except for the combustion chamber, which is made from superalloys due to the high temperatures (1920°K), being cooled by the cooling air. A portion of the cooling air penetrates the bores in the wall of the combustion chamber, creating a peripheral layer of drag air for dragging the molten ashes and particulates.

One of the main characteristics of the gas turbines is their versatility with regard to fuels, operating with gases such as natural gas, evaporated oils and process gases (refineries, blast-furnaces and gasifiers); liquids such as clean liquids that are volatile Naphthas, light distillates (Diesel, kerosene) and viscous and heavy residual oils; and solids. Liquid fuels with high ash contents (crude and residual oils) require cleaning equipment prior to their utilization.

Table 7 illustrates the properties of the three types of conventional fuels and of the catalytic cellulignin. The latter is placed between the natural gas and light distillates (clean fuels) and the mixtures of heavy distillates and low-ash crude oil. It does not contain V<sub>2</sub>O<sub>5</sub>, WO<sub>3</sub>, MO<sub>3</sub>, or Pb, and the S content is very low. The Na

+ K for the clean catalytic cellulignin concentration is:close to that of the clean fuels while for normal catalytic cellulignin it is close to that of heavy residual high-ash crude oils (table 8). The pre-hydrolysis carried out with deionized water is an effective technology of producing the clean catalytic cellulignin as a fuel for gas turbines. The only parameter out the conditions of clean fuel is the total ash contents (< 0.1%). These are, however, significantly reduced in the cyclone, reaching total particulate contents < 200ppm, and contents lower than 8ppm for particles with size bigger than 5μm.

Natural gas distillates do not need a fuel treatment. Mixtures of heavy
distillates, low-ash crude oils and especially heavy residual high-ash crudes need
washing of the fuel that is based on the water-solubility of sodium, potassium, and
calcium. There are four conventional washing processes, namely: centrifuge, D.C.
electric, A.C. electric, and hybrid. The catalytic cellulignin dispenses with any washing process that has been used for reducing the Na + K contents from 100ppm down
to levels of from 5 to 0.5ppm in crude and residual oils.

Heavy Crude

0,92/1,05

100/1800

10,0/12,5

1/350 5/400 0/25,0

0,5/0,4

100/1000

42,3/43,7

Cellu- Mixtures of Distillates a Low Ash High Ash Crudes Residures 79/129 -9/35 0,8786 12,40 1,075 Heavy Distillates 42,1 6,20 92 Typical Crude from 2,2/4,5 0/1,0 36 2/10 0,15 Libia 42,2 0,84 20 2,3 Ash 12,0/13,2 43,9/44,8 20 a 200 0,80/0,92 0,1/2,7 Low 0,3/3 0/20 0/15 -9/43 2/100 10/93 Any (3) (4) Normal 350 (2) 2000 Zero Zero 280 PPm 4,3 20,0 **09**> 0,50 <80 ppm Catalytic lignin Any (3) 350 (2) Clean 1000 Zero Zero <500 0,50 4,3 <T.A. (1) 0,7545 (5) 14,75 0,047 20,0 53,2 0,79 35,0 0,82/0,88 12,0/13,2 43,9/45,3 0 a 20 0,03/0,3 0,164 a 0,1/0,8 0,293 2,0/4,0 0,1/0 0/2/0 0/1/0 0/0,1 Oil #2 66/93 -23/-1 Distillates and Naphtha -48/-12 48/104 12,83 0,104 0/2/0 0,001 42,3 0,85 34,4 38,1 2,48 2,67 #2 Table 7: Properties of the Fuels 0,01/0,1 0,01/01 1.4/2.2 0/0'2 0/1,5 1 a 5 0,0 Kero-44,6/ 45,5 12,8 14,5 sene 54/71 - 45 0,78/ 0,83 Calorific Power MJ/kg Sécof Desn. at 38°C Visc. CS to 38 ° C Flow Point (°C) Flash Point (°C) Coal Residues Na + K (ppm) Sulfure (%) Vanadium Hydrogen Properties Lead Calcium Grau API Ashes SSU

Properties	Distillates and	and Catalytic Cellulianin	Mixtures of Distillates and	Mixtures of Distillates and High Ash Critic and Heavy Beel.
	Naphtha		Low Pressure Crude	dues
Preheating of the fuel	No	O.Z.	Yes	Yes
Atomization	Mechanics/ Low No Pressure Air	O.	Low Pressure/ High Pressure Air	High Pressure Air
Disalination	No	000	Some	Yes
Inhibitor	No	No (Limited)	Limited	Always
Washing of the Tur- bine	O.	No	Yes (except for distillate)	Yes
Initial Fuel	With Naphiha	Ignition (GLP, natural Some Fuels gas, heated tubes, elec- tric resistance)	Some Fuels	Always
Cost	Higher	Intermediate	Intermediate	Lower
Description	Low-quality Distillate free of ashes	stillate Porous powder with Low Ash, Lir limited ash contents, Contaminants that can be reduced by cyclones	nited Level	of High Ash Low Volatility
Designation ASTM	1GT, 2GT, 3GT	(3-GT)	3GT	46T
Turbine Inlet Tem- Higher Perature	Higher	Intermediate	Intermediate	Low

<u>Table 8 –</u> Inorganic impurities (mg/g) of Eucalyptus. Catalytic Cellulignin and Prehydrolysate

	Ca	K	Na	Mg	Р	Al	Si	Mn	Fe	Zn	S
Eucalipto	560	400	<140	160	170	50	<120	20	10	ND	140
Celulignina normal (1)	500	<60	<140	<40	10	<40	<120	<4	<10	<6	<80
Celulignina limpa (2)	<53	<5	<1	<60	<2	<40	<120	<2	<7	<b>ح</b> 4	<80
Pré-hidroli- sado (3)	260	370	80	140	65	10	25	20	8	5	1950

(1)cellulignin processed with filtered tap water, with X-rays semi-qualitative analysis
(2)cellulignin processed with deionized, with X-rays semi-qualitative analysis except for K (by ICP/AES) and Na (AAS-flame)

(3)mass balance not carried out due to the absence of initial water and washing water analysis.

For gas turbines, specifications of the fuel level are usually made. In the case of catalytic cellulignin, due to the purification of the cyclones coupled to the combustor outside the turbine, the specifications should be made at the level of the combustion gases or in terms of an "equivalent fuel".

The influence of the (Na + K) contents (ppm) on the working temperature of the Iconel superalloy 718 is given by:

(Na + K) ppm	0,33	2,28	3,70	4,89	5,65
Temperature (°C)	927	871	815	760	704

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The catalytic cellulignin fuel allows operation in the range of 800 to 830°C. Coatings are utilized in order to increase the resistance of the superalloys to hot corrosion. Table 8 shows the main types of coating obtained by diffusion (Al, Pt, Rh, NiCrSi) and by overlayers (Co, Cr, Al, Y). Various techniques of depositing the overlayers are utilized, namely: plasma spray, sputtering, deposition of vapor by electronic beam (PVD) and cladding. At present, the hot-corrosion resistances are limited by the coatings and not by the base-metals of the rotors and stators of the turbines.

The protection with plasma or EB/PVD, however, enables one to achieve 16000h of operation, even under aggressive conditions.

The main requirements for a gas turbine fuel are: calorific power, cleanliness, corrosivity, deposition/obstruction and availability. The fuel from clean catalytic cellulignin obtained by pre-hydrolysis from biomass with deionized water meets all the above requirements.

Table 9: Protecting Layers (coatings) of the Turbines

Specification of	Element	Deposit.	Typical applications	Capacity in hours;
the Protection	in the	technique		Combustion
	Layer		·	chamber (870°C)
UC	Al	PC	Co Base stators of	·
870	Al,Si	PC	Base parts Ni	
RT-5	Al,Cr	DPC	Ni Base stators	·
RT-17	Al,Ni	DPC	Nickel doped with	
			Thorium	·
RT-19	Al	DPC	Co Base stators	
			(High temperature	·
			service)	
RT-21	Pt,Al	PC	Ni stators and rotors	800
RT-22	Rh,Al	EP/PC	Ni base rotors	5000
BB	Pt,Rh,Al	EP/PC	Ni and Co Base sta-	
·			tors and rotors	·
RT-44	Co,Cr,Al,	EB/PVD	Co Base stators	
·	Y		•	
Overlayers	Ni,Co,Cr,	EB/PVD	Overlayers for vari-	7000 (plasma)
	Al		ous services	14000 (composed
			Υ,	plasma)
				18000 (clad)

PC – Pack Cementation; DPC – Double Pack Cementation; EP – Eletroplating; EB - Electron Beam; PVD – Physical Vapor Deposition

### CLAIMS

- 1. A catalytic cellulignin fuel, characterized in that it is composed of cellulose and globulized lignin with specific surface of about 1.5 2.5 m²/g.
- A catalytic cellulignin fuel according to claim 1, characterized in that it is
   composed of cellulose and globulized lignin with an average specific surface of about 2 m²/g.
  - 3. A cellulignin fuel according to claim 1 or 2, characterized in that it has a heat combustion value of about 18 to 20 MJ/kg.
  - 4. A cellulignin fuel according to any one of claims 1 to 3, characterized in that it is ground into particles having size lower than 250 mm.
- 5. A cellulignin fuel according to any of the preceding claims, characterized in that it presents an ignition time equal to or shorter than 20 ms (0.02s).
  - 6. A cellulignin fuel according to any one of the preceding claims, characterized in that it has a volatilization temperature of about 350° C.
- 7. A cellulignin fuel according to any one of the preceding claims, characterized by a Na + K content lower then or equal to 5 ppm.
  - 8. A cellulignin fuel according to any one of the preceding claims, characterized in that it generates combustion gases with total particulates lower than 200 ppm, the particles having diameter lower than 5 nm at concentrations lower than 8 ppm.

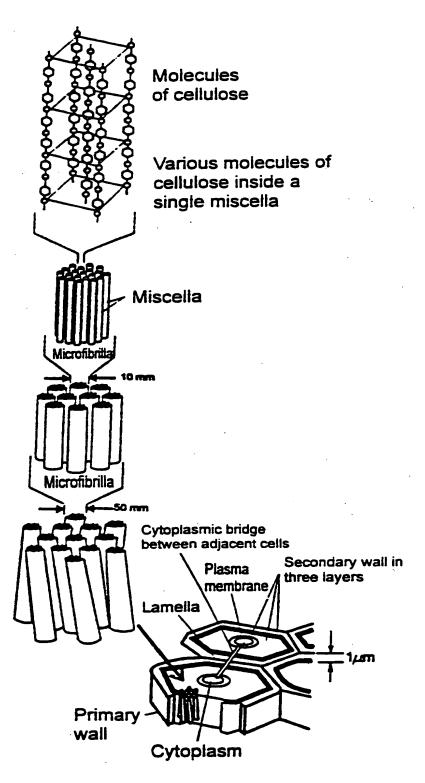
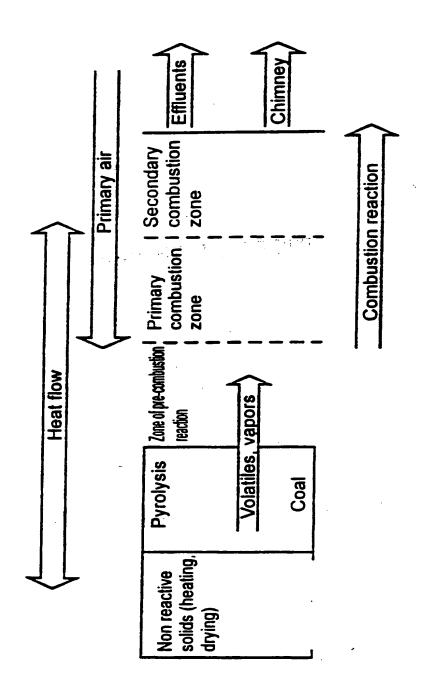


FIG 1 Cellular structure of biomass



**:** |G| 2 solid fuels.

Complexity of the combustion of wood



Fig 3a

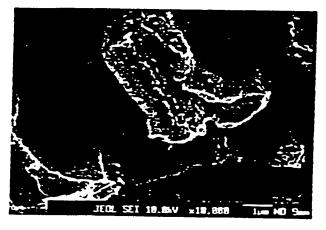


Fig 3b

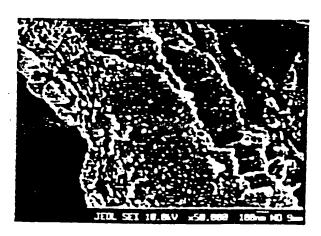


Fig 3c



Fig 3d

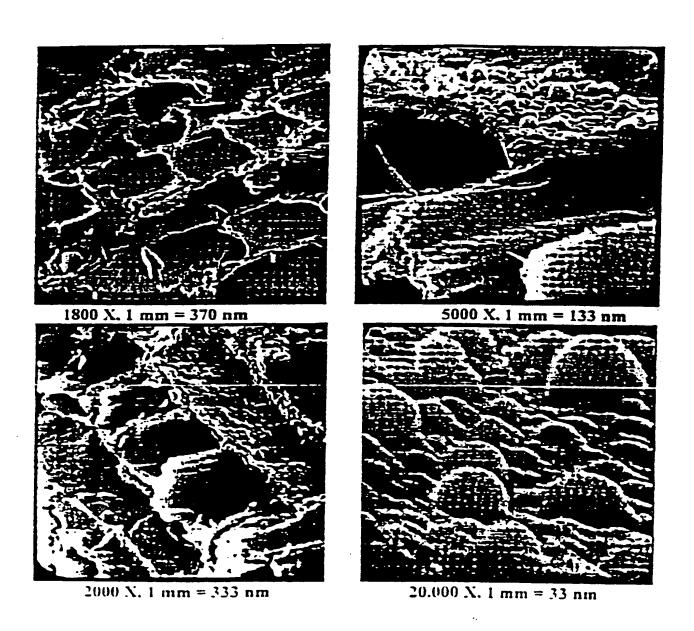


Fig 3e: Microstructure of the cellulignim with globalized lignim

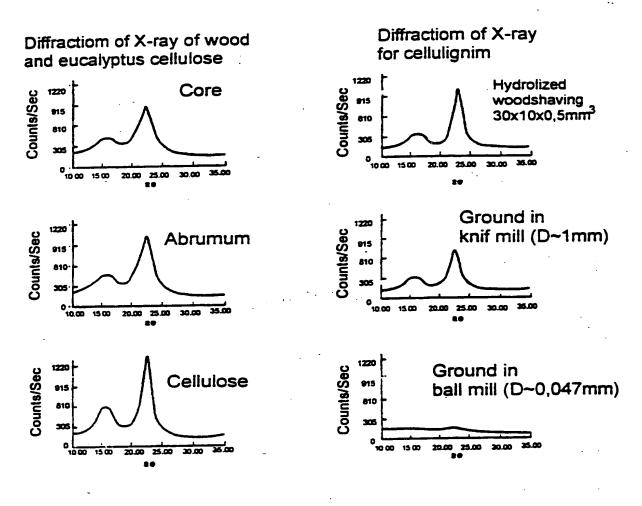


FIG 4 x-Ray diffratogram for wood, cellulose and cellulignin

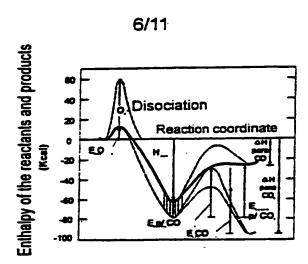


FIG 5 Variation of the Enthalpy of the Reactants and products the coordinate of the Carbon-Oxygen reaction.

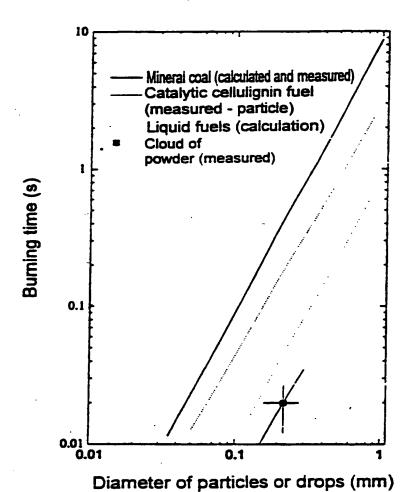


FIG 6 Burning time versus Diameter of particle for mineral coal, catalytic cellulignin fuel, particle and in powder cloud and liquid fuels

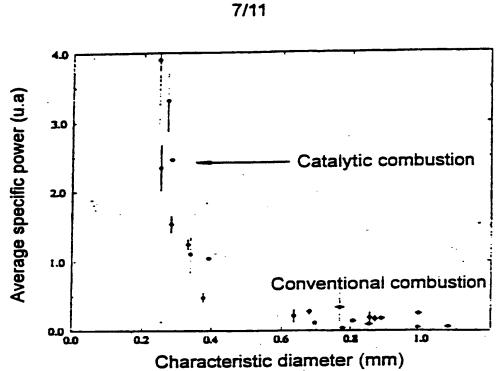


FIG 7a Average specific power irradiated in the combustion a Catalytic Cellulignin particle (linear scale)

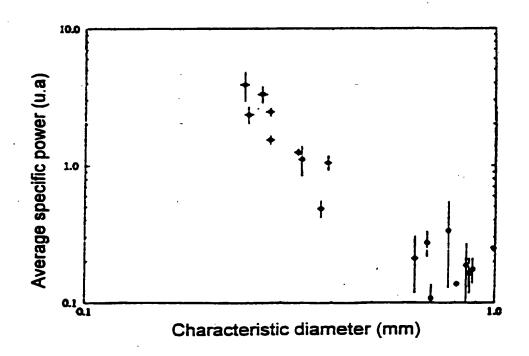


FIG 7b Average specific power irradiated in the combustion a catalytic cellulignin particle (logarithmic scale)

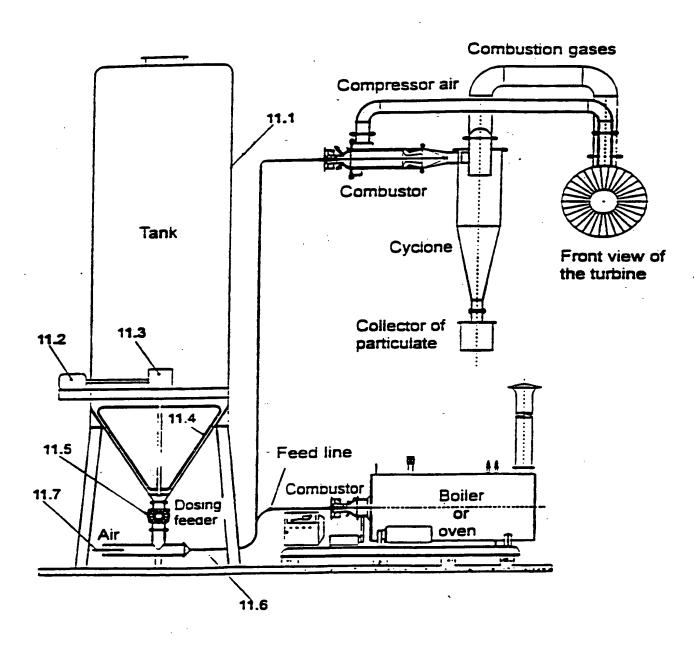


FIG 8 Catalytic Cellulignin feeding system for Boilers/Ovens or gas turbines

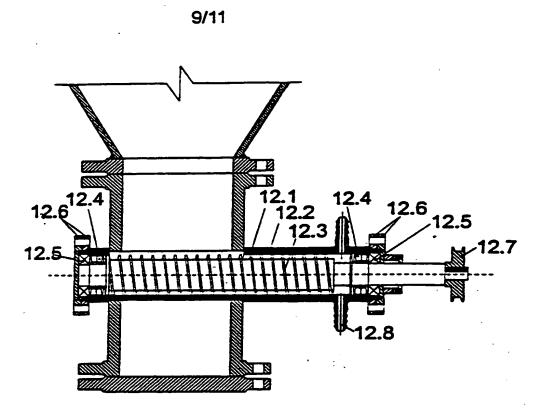


FIG 9 Helical feeder

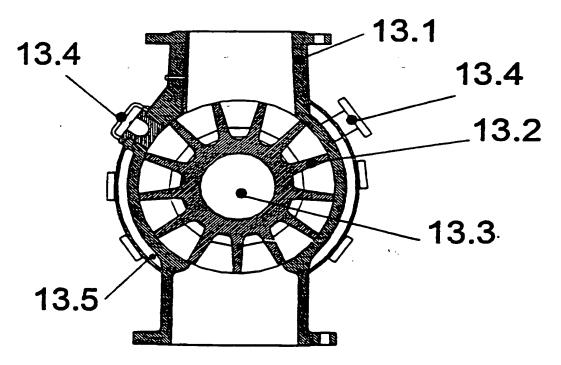


FIG 10 Rotary valve

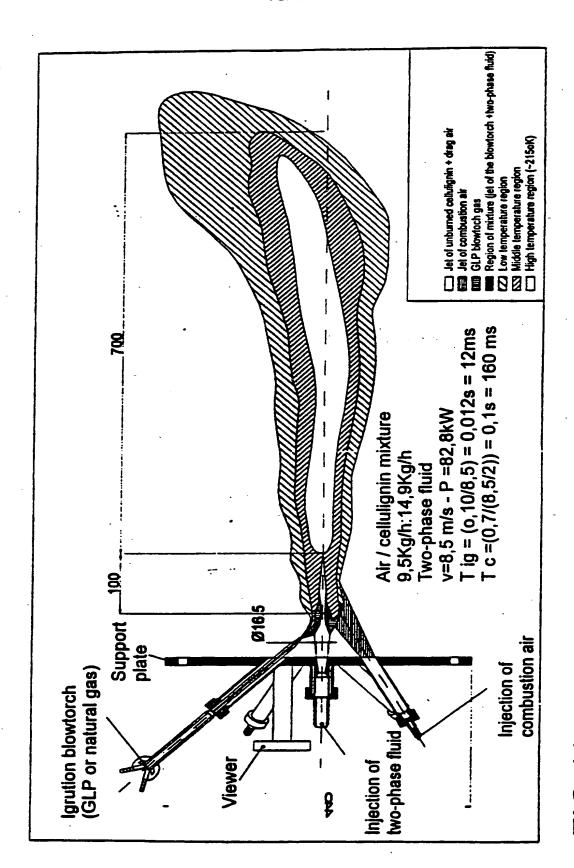


FIG 11 Axial combustor with flame of cellulignin in an open environment

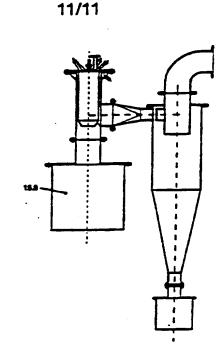


FIG 12a Combustor for cellulignin, cycloning and collection of particulates (horizontal)

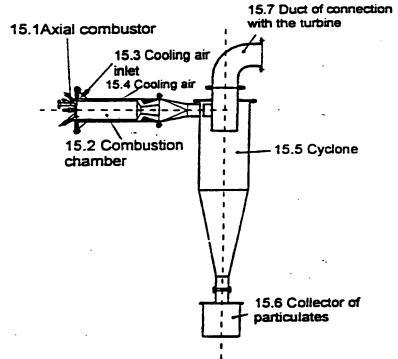


FIG 12b Combustor for cellulignin, cycloning and collection of particulates (vertical)

# INTERNATIONAL SEARCH REPURT

PCT/BR 00/00066

A CLASSIFICATION OF SUBJECT MATTER  IPC 7 C10L5/44					
According to	o International Patent Classification (IPC) or to both national classific	estion and IPC			
	SEARCHED				
Minimum de	ocumentation searched (classification system followed by classification C10L C13K D21B D21C	Jon symbols)			
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	ternal, WPI Data, PAJ, COMPENDEX		<u></u>		
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, <u> </u>		• .			
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	en the prority date claimed	*8.* document member of the same patent t			
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# **PCT**

## REQUEST

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23 JUN 2000 23 - 8 - 90 Naternational Filing Date	
INITION AFFLICATION  Name of receiving Office and "PCT International Application	эп <sup>ээ</sup>

The undersigned requests that the present international application be processed according to the Patent Cooperation Treaty. or agent's file reference (if desired) (12 characters maximum) PE-3848 Box No. I TITLE OF INVENTION "CATALYTIC CELLULIGNIN FUEL" **APPLICANT** Box No. II Name and address: (Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country. The country of the address indicated in this Box is the applicant's State (that is, country) of residence if no State This person is also inventor. of residence is indicated below.) Telephone No. RM MATERIAIS REFRATÁRIOS LTDA. Estrada do Pinhal, 750 Facsimile No. 12600-000 - Lorena Brazil Teleprinter No. State (that is, country) of nationality: State (that is, country) of residence: BR BR This person is applicant all designated States all designated States except the United States of America the United States of America only the States indicated in the Supplemental Box for the purposes of: Box No. III FURTHER APPLICANT(S) AND/OR (FURTHER) INVENTOR(S) Name and address: (Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country. The country of the address indicated in this Box is the applicant's State (that is, country) of residence if no State This person is: of residence is indicated below.) applicant only GARCIA PINATTI, DALTRO applicant and inventor Rua Oswaldo Aranha, 1194, casa 1, Vila Zelia inventor only (If this check-box Lorena, São Paulo is marked, do not fill in below.) Brazil State (that is, country) of nationality: State (that is, country) of residence: BR This person is applicant all designated States except the United States of America all designated the United States the States indicated in the Supplemental Box for the purposes of: of America only Further applicants and/or (further) inventors are indicated on a continuation sheet. Box No. IV AGENT OR COMMON REPRESENTATIVE; OR ADDRESS FOR CORRESPONDENCE The person identified below is hereby/has been appointed to act on behalf of the applicant(s) before the competent International Authorities as: agent common representative Name and address: (Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.) Telephone No. (21) 553-1811 DANNEMANN, SIEMSEN, BIGLER & IPANEMA MOREIRA Caixa Postal 2142 Facsimile No. Rua Marquês de Olinda, 70 (21)553-1812 553-1813 Botafogo 22251-040 - Rio de Janeiro - RJ Teleprinter No. Address for correspondence: Mark this check-box where no agent or common representative is/has been appointed and the space above is used instead to indicate a special address to which correspondence should be sent.

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Name and address: (Family name followed by given name: for a le designation. The address must include postal code and name of coun address indicated in this Bax is the applicant's State (that is, country) of residence is indicated below.)  VIEIRA, CHRISTIAN ALEXANDRE  Av. Andrade Neves, 710, apto. 33  Centro Campinas, São Paulo Brazil	gal entity, full official
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Sheet No. 03

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Preca design from	utionary Designation Statement: In addition to the designations which would be permitted under the PCT except and the scope of this statement. The applicant declares that the statement is not confirmed before the expiration of 15 more expiration of that time limit. (Confirmation (including fees) must be statement.	hose	esigna addit	tional designate designates de	ations are stee is to be re	ubject garded	to confirmation and that any

Sheet No. ....

Further priority Clain sale noncated in PRIORITY CLAIM Box No. VI Where earlier application is: Number Filing date of earlier application regional application:\* international application: national application: of earlier application regional Office receiving Office (day/month/year) country item (1) BR PI 9902606-6 23 June 1999 (23.06.99)item (2) item (3) The receiving Office is requested to prepare and transmit to the International Bureau a certified copy of the earlier application(s) (only if the earlier application was filed with the Office which for the purposes of the present international application is the receiving Office) identified above as item(s): \* Where the earlier application is an ARIPO application, it is mandatory to indicate in the Supplemental Box at least one country party to the Paris Convention for the Protection of Industrial Property for which that earlier application was filed (Rule 4.10(b)(ii)). See Supplemental Box. INTERNATIONAL SEARCHING AUTHORITY Box No. VII Request to use results of earlier search; reference to that search (if an earlier Choice of International Searching Authority (ISA) (if two or more International Searching Authorities are competent to carry out the international search, indicate the Authority chosen; the two-letter code may be used): search has been carried out by or requested from the International Searching Authority): Country (or regional Office) Date (day/month/year) Number ISA/ **EPO** Box No. VIII CHECK LIST; LANGUAGE OF FILING This international application is accompanied by the item(s) marked below: This international application contains the following number of sheets: 1. Tee calculation sheet 2. separate signed power of attorney description (excluding copy of general power of attorney; reference number, if any: 36 sequence listing part) statement explaining lack of signature 01 claims 5. priority document(s) identified in Box No. VI as item(s): 01 abstract 6. Translation of international application into (language): 11 drawings 7. 

separate indications concerning deposited microorganism or other biological material sequence listing part of description 8. nucleotide and/or amino acid sequence listing in computer readable form 53 9. dther (specify): Total number of sheets: Language of filing of the Figure of the drawings which English international application: 7a should accompany the abstract: SIGNATURE OF APPLICANT OR AGENT Box No. IX Are the name of the person signing and the capacity in which the person signs (if such capacity is not obvious from reading the request). nemann, Siemsen, Bigler & Ipanema Moreira (Raul Hey) For receiving Office use only Drawings: Date of actual receipt of the purported international application: received: Corrected date of actual receipt due to later but timely received papers or drawings completing the purported international application: not received: Date of timely receipt of the required corrections under PCT Article 11(2): Transmittal of search copy delayed International Searching Authority ISA/ until search fee is paid. (if two or more are competent): For International Bureau use only Date of receipt of the record copy by the International Bureau:

Form PCT/RO/101 (last sheet) (July 1998; reprint January 2000)

See Notes to the request form

This sheet is not part of and does not count as a sheet of the international application.

PCT	For receiving Office use only
FEE CALCULATION SHEET Annex to the Request	International application (No.) / 0 0056
Applicant's or agent's file reference PE-3848	Date stamp of the receiving Office
Applicant RM MATERIAIS REFRATÁRIOS LTDA. et al	
CALCULATION OF PRESCRIBED FEES	
1. TRANSMITTAL FEE	236,00 T
2. SEARCH FEEDEM . 4.6.2 . 0.7 . x . 0 . 8.7.6.3.6.3 .  International search to be carried out by EPO  (If two or more International Searching Authorities are competent in relation application, indicate the name of the Authority which is chosen to carry out the international searching Authority which is chosen to carry out the international searching application.	m to the international search.)
Basic Fee The international application contains 53 sheets.	
first 30 sheets CHF .650 x 1.10502	, 26 bi
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MODE OF PAYMENT	
authorization to charge deposit account (see below)  cheque  postal money order  bank draft  X cash  revenue stamps	coupons other (specify):
DEPOSIT ACCOUNT AUTHORIZATION (this mode of payment may	y not be available at all receiving Offices)
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Deposit Account No. Date (day/month/war)	S:

Signature

Date (day/month/year)

form PCT/RO/101 (Annex) (January 2000)

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# From the INTERNATIONAL SEARCHING AUTHORITY

To:
DANNEMANN, SIEMSEN, BIGLER &
IPANEMA MOREIRA
Rua Marques de Olinda 70, Botafogo
Caixa Postal 2142
22251-040- Rio de Janeiro - RJ

PCT 33-13.00

NOTIFICATION OF TRANSMITTAL OF THE INTERNATIONAL SEARCH REPORT OR THE DECLARATION

(PCT Rule 44.1)

BRAZIL	
	Date of mailing (day/month/year) 13/10/2000
Applicant's or agent's file reference PE-3848	FOR FURTHER ACTION See paragraphs 1 and 4 below
International application No. PCT/BR 00/ 00066	International filing date (day/month/year) 23/06/2000
Applicant	
RM MATERIAIS REFRATARIOS LTDA.	

1.	$\mathbf{x}$	The appli	icant is hereby n	otified that the International Search Report has been established and is transmitted t	erewith.	
		Filling of	amendments s	and statement under Article 19:		_
		The appli	cant is antitled	if he so wishes, to amend the claims of the International Application (see Rule 46):		•
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		)4/h0	The sime limit to	or filing such amendments is normally 2 months from the date of transmittal of the		
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3.	$\Box$	With reg	ard to the prote	est against payment of (an) additional fee(s) under Rule 40.2, the applicant is notifie	d that	
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		the	protest togethe	r with the decision thereon has been transmitted to the International Bureau together	With the	
		app	olicant's request	to forward the texts of both the protest and the decision thereon to the designated Of	iices.	
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		no	decision has be	en made yet on the protest; the applicant will be notified as soon as a decision is made	æ.	
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4.	Furt	her action	n(s): The app	licant is reminded of the following:		
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	Sho	rtly after 1	8 months from	the priority date, the international application will be published by the International Bu	of the	
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	wi	shes to po	stpone the entr	into the national phase until 30 months from the priority date (in some Offices even	iaioi).	
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NL-2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
Fax: (+31-70) 340-3016

Authorized officer

Toñi Muñoz-Manneken

Form PCT/ISA/220 (July 1998)

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# NOTES TO FORM PCT/ISA/220

These Notes are intended to give the basic instructions concerning the filing of amendments under article 19. The Notes are based on the requirements of the Patent Cooperation Treaty, the Regulations and the Administrative Instructions under that Treaty. In case of discrepancy between these Notes and those requirements, the latter are applicable. For more detailed information, see also the PCT Applicant's Guide, a publication of WIPO.

In these Notes, "Article", "Rule", and "Section" refer to the provisions of the PCT, the PCT Regulations and the PCT Administrative Instructions respectively.

# INSTRUCTIONS CONCERNING AMENDMENTS UNDER ARTICLE 19

The applicant has, after having received the international search report, one opportunity to amend the claims of the international application. It should however be emphasized that, since all parts of the international application (claims, description and drawings) may be amended during the international preliminary examination procedure, there is usually no need to file amendments of the claims under Article 19 except where, e.g. the applicant wants the latter to be published for the purposes of provisional protection or has another reason for amending the claims before international politication. Furthermore, it should be emphasized that provisional protection is available in some States only.

# What parts of the international application may be amended?

Under Article 19, only the claims may be amended.

During the international phase, the claims may also be amended (or further amended) under Article 34 before the International Preliminary Examining Authority. The description and drawings may only be amended under Article 34 before the International Examining Authority.

Upon entry into the national phase, all parts of the international application may be amended under Article 28 or, where applicable, Article 41.

### When?

Within 2 months from the date of transmittal of the international search report or 16 months from the priority date, whichever time limit expires later. It should be noted, however, that the amendments will be considered as having been received on time if they are received by the International Bureau after the expiration of the applicable time limit but before the completion of the technical preparations for international publication (Rule 46.1).

### Where not to file the amendments?

The amendments may only be filed with the International Bureau and not with the receiving Office or the International Searching Authority (Rule 46.2).

Where a demand for international preliminary examination has been its filed, see below.

#### How?

Either by cancelling one or more entire claims, by adding one or more new claims or by amending the text of one or more of the claims as filed.

A replacement sheet must be submitted for each sheet of the claims which, on account of an amendment or amendments, differs from the sheet originally filed.

All the claims appearing on a replacement sheet must be numbered in Arabic numerals. Where a claim is cancelled, no renumbering of the other claims is required. In all cases where claims are renumbered, they must be renumbered consecutively (Administrative Instructions, Section 205(b)).

The amendments must be made in the language in which the international application is to be published.

### What documents must/may accompany the amendments?

Letter (Section 205(b)):

The amendments must be submitted with a letter.

The letter will not be published with the international application and the amended claims. It should not be confused with the "Statement under Article 19(1)" (see below, under "Statement under Article 19(1)").

The letter must be in English or French, at the choice of the applicant. However, if the language of the international application is English, the letter must be in English; if the language of the international application is French, the letter must be in French.

# NOTES TO FORM PCT/ISA/220 (continued)

The letter must indicate the differences between the claims as filed and the claims as amended. It must, in particular, indicate, in connection with each claim appearing in the international application (it being understood that identical indications concerning several claims may be grouped),whether

- the claim is unchanged;
- (ii) the claim is cancelled;
- (iii) the claim is new;
- (iv) the claim replaces one or more claims as filed;
- (v) the claim is the result of the division of a claim as filed.

# The following examples illustrate the manner in which amendments must be explained in the accompanying letter:

- [Where originally there were 48 claims and after amendment of some claims there are 51]:
   "Claims 1 to 29, 31, 32, 34, 35, 37 to 48 replaced by amended claims bearing the same numbers; claims 30, 33 and 36 unchanged; new claims 49 to 51 added."
- [Where originally there were 15 claims and after amendment of all claims there are 11]:
   "Claims 1 to 15 replaced by amended claims 1 to 11."
- 3. [Where originally there were 14 claims and the amendments consist in cancelling some claims and in adding new claims]:
  "Claims 1 to 6 and 14 unchanged; claims 7 to 13 cancelled; new claims 15, 16 and 17 added." or
  "Claims 7 to 13 cancelled; new claims 15, 16 and 17 added; all other claims unchanged."
- 4. [Where various kinds of amendments are made]: "Claims 1-10 unchanged; claims 11 to 13, 18 and 19 cancelled; claims 14, 15 and 16 replaced by amended claim 14; claim 17 subdivided into amended claims 15, 16 and 17; new claims 20 and 21 added."

# "Statement under article 19(1)" (Rule 46.4)

The amendments may be accompanied by a statement explaining the amendments and indicating any impact that such amendments might have on the description and the drawings (which cannot be amended under Article 19(1)).

The statement will be published with the international application and the amended claims.

It must be in the language in which the international appplication is to be published.

It must be brief, not exceeding 500 words if in English or if translated into English.

It should not be confused with and does not replace the letter indicating the differences between the claims as filed and as amended. It must be filed on a separate sheet and must be identified as such by a heading, preferably by using the words "Statement under Article 19(1)."

It may not contain any disparaging comments on the international search report or the relevance of citations contained in that report. Reference to citations, relevant to a given claim, contained in the international search report may be made only in connection with an amendment of that claim.

### Consequence if a demand for international preliminary examination has already been filed

If, at the time of filing any amendments under Article 19, a demand for international preliminary examination has already been submitted, the applicant must preferably, at the same time of filing the amendments with the International Bureau, also file a copy of such amendments with the International Preliminary Examining Authority (see Rule 62.2(a), first sentence).

### Consequence with regard to translation of the international application for entry into the national phase

The applicant's attention is drawn to the fact that, where upon entry into the national phase, a translation of the claims as amended under Article 19 may have to be furnished to the designated/elected Offices, instead of, or in addition to, the translation of the claims as filed.

For further details on the requirements of each designated/elected Office, see Volume II of the PCT Applicant's Guide.



# **PCT**

# INTERNATIONAL SEARCH REPORT

(PCT Article 18 and Rules 43 and 44)

Applicant's or agent's file reference	FOR FURTHER See Noti (Form PC	ification of Transmittal of International Search Report CT/ISA/220) as well as, where applicable, item 5 below.							
PE-3848	International filing date (day/month/)	(year) (Earliest) Priority Date (day/month/year)							
International application No.									
PCT/BR 00/00066	23/06/2000	23/06/1999							
Applicant									
RM MATERIAIS REFRATARIOS	LTDA.	· .							
This International Search Report has be-	en prepared by this International Searc	ching Authority and is transmitted to the applicant							
according to Article 18. A copy is being t	transmitted to the International Bureau.								
This International Search Report consist	ts of a total of2 sheeps a copy of each prior art document cite								
X It is also accompanied b	ע ב עט פין or each phor an document cit								
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a With regard to the language, th	e international search was carried out o	on the basis of the international application in the							
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2. Certain claims were fo	ound unsearchable (See Box I).								
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C. DOCUME	ENTS CONSIDERED TO BE RELEVANT		
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			1.0
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	ent defining the general state of the art which is not	or priority date and not in conflict with to cited to understand the principle or the	he application but
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	nent published prior to the international filing date but than the priority date claimed	"&" document member of the same patent	
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	4. O-t-b 2000	13/10/2000	
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Name and	mailing address of the ISA	Authorized officer	
	European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk		
	Tel. (+31-70) 340-2040, Tx. 31 651 epo nl. Fax: (+31-70) 340-3016	Zuurdeeg, B	

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> PCT - Chapter II MU DG2

Code: 311878002

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Erhardstrasse 27

D-80298 München

DE-Alemanha

Att.: International Preliminary

**Examining Authority** 

Examiner: Van Iddekinge, R

Rio. June 20, 2001

PCT - International Application PCT/BR00/00066 Ref.:

filed on June 23, 2000

RM MATERIAIS REFRATÁRIOS LTDA.

Our ref.: PE-3848 (MCB)

Dear Sirs,

In response to the first written opinion issued on the above case, applicant respectfully submits that the present application meets both novelty and inventive requirements over the prior art references D1, D2, D3 and D4.

Claims 1 to 8 were rejected under the assumption that D1 to D4 would disclose the same process steps for treating biomass nd that the resulting product of said processes would be identical to the cellulignin fuel defined in the present application. As it will be clarified below, the present invention is a cellulignin product comprising specific, distinct and unexpected characteristics which is obtained through a process involving different parameters when compared to the prior art.

Firstly it is noticed that a detailed description of the presently claimed solid cellulignin structure and its catalytic (fuel) characteristics is presented throughout the specification with reference to the illustrative drawings.

US Pat 5,338, 366 (D1) relates to a process of pre-hydrolysis of biomass which is described as a preliminary method for other techniques for treating biomass such as

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hydrolysis of cellulose, paper pulp production, alcohol and furfural production and others. It must be stressed the referred to patent describes the resulting solid in the

form of a slurry containing the swollen biomass and does not make any mention of the obtention of a solid product that could present the same features as presently claimed nor the use of that solid as a fuel, which is the key point of the present invention.

A brief summary of the method proposed in the above US patent is presented below:

- a) mixing the biomass with amineral acid (0.5 3% 54 at 65°C) forming a slurry with a consistency that guarantees the biomass wetability by the acid in sufficient concentration (8 - 12% of solids) for eventually hydrolyzing the hemicellulose;
- b) dewatering of the slurry (35 50% of solids) in a screw press for minimizing the necessary amount of steam and maintaining the sugar concentration at reasonable levels in the following stages of the pre-hydrolysis;
- heating the dewatered slurry by directly contacting it with steam up to the reaction temperature and pressure; the pre-hydrolysis is carried in a tower-type vertical reactor (conventional) at a temperature of from 121 - 177° C, under the pressure of from 2.1 to 3.6 atm., for 2 - 40 minutes. This stage takes place at the top of the rector with a consistency of 34% at the top and 24% at the bottom. In order to withdraw the solid/pre-hydrolysate mixture at the outlet of the reactor bottom, a dilution and cooling of the pre-hydrolysate until 8 - 12% of consistency and temperature of 82°C.
- d) retaining the biomass of the dewatered slurry in those temperature and pressure conditions for a time sufficient for the hemicellulose pre-hydrolysis.
- e) adding mineral acid to the liquid resulting from the dewatered from the screw press (pressate);
- heating the liqueur/acid mixture;
- g) using the liqueur/acid mixture as a source of acidic solution in stage (a);
- h) the liqueur/acid mixture is preheated up to 55° C (stage f) in an indirect heat exchanger that is heated by the final pre-hydrolysate resulting from the prehydrolysis stage.

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A fluffer may be used between the stages (b) and (c) for fluffing the biomass at the inlet of the tower-type vertical pre-hydrolysis reactor.

As can be seen from the above summary, the process steps described in reference D1 (US5,338,366) do not anticipate nor foresee the specific parameters now disclosed in the present application nor the final solid product thus obtained.

Patent GB Pat 1569238 (D2) relates to "an extremely light pre-hydrolysis" with acid contents lower than 1% and temperature lower than 160°C (reactor coated with Teflon). The object of that patent is the obtention of cellulose pulp with recovery of the monosaccharides generated by the decomposition of hemicellulose. In fact, since the main objective of GB Pat 1569138 is to obtain a cellulose pulp, the acidic process should be as mild as possible, so that there will not be any damage to the cellulose fiber, in order not to affect its mechanical strength.

According to the present invention, however, the object is exactly the opposite, that is to say, a pre-hydrolysis with intermediate amounts of sulfuric acid (1 - 2%) and at intermediate temperature range (160 - 170 °C) with the purpose of generating the macromolecular porosity to achieve a catalytic combustion (direct interaction of oxygen with carbon similar to natural gas). Consequently, the resulting product from the process claimed in D2 is distinct from the cellulignin according to the present application.

The following comparative text illustrates the two distinct kinds of hydrolysis. Only in the case of the present invention the process is carried out at intermediary conditions, which requires more simple reactors and parameters (batch processing, coating of the reactors with refractory metals (Ti, Nb, Ta and alloys thereof), average acid contents (1 − 2%), average temperatures (160 − 170°C), short times (20 − 30 minutes)):

(Total hydrolysis in 1st and 2nd stages) = Light pre-hydrolysis; GB Pat 1569138 obtention of pulp with cellulose fibers without fractures or pores; recovery of carbohydrates from the hemicelluloses; polysacharides digestion; no worry about obtaining a solid with microstructure with macromolecular porosity.



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Agente da Propriedade Industrial Registro nº 192

Associado à A.B.A.P.I. pe3848ep0

Present invention = Medium pre-hydrolysis; main objective: solid with microstructure with macromolecular porosity in the cellulignin; average contents of acid; average temperatures; short reaction time

Patent US 5366558 (D3) deals with the classic process of "total hydrolysis" in two steps aiming at the total decomposition of carbohydrates and according to which there is no worrying about the preservation of a solid material and much less worrying about creating a porous microstructure at macromolecular (catalytic) level therein (the solid is actually referred to "residue" - column 22 line 46). Therefore, this patent text clearly indicates that a solid product as claimed in the present application could not be obtained by that process.

The process disclosed in Pat. 5,366,558 presents the following characteristics in its first stage which are distinct from the process used to prepare the cellulignin of the present invention:

According to the above patent a continuous process is used wherein a significant complexity is required for the equipment and for the flows of liquids. In the present application, on the other hand, it is disclosed a batch process aiming at the simplicity of the equipment and of the flows of liquids. Due to its enormous complexity, the equipment described in Pat 5,366,558 can only be manufactured from stainless steel or nickel alloys (column 9 line 56), for which reason acidic solutions with pH between 2.0 and 3.0 (column 1 line 35) are used. Solutions with lower pH (~ 1) would cause serious corrosions.

The drawbacks of the pre-hydrolysis (1st stage) of Pat 5,366,558 due to the abovementioned factors makes it necessary to produce large surfaces for implementing the processes of the second stage by a disintegrator (column 3 line 60), to eliminate the deficiencies of the first stage. Although Pat 5,366,558 does not ontain any quantitative information on the granulometry achieved in the disintegrator, it generates macroscopic particles having surfaces considerably larger than the surface generated by the macromolecular porosity (catalytic) obtained according to the present invention.

In summary, Pat 5,366,558 does not provide for equipments (materials), processes and characterization of the cellulignin microstructure after the first stage because its objective is the total disintegration of the solid in the subsequent stage. In



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dade Industria Registro nº 192

Associado à A.B.A.P.I

pe3848ep

present invention, on the other hand, the pre-hydrolysis (first stage) process was extended to obtain a microstructure with macromolecular porosity for achieving a catalytic combustion, said microstructure being not described nor foreseen in the above mentioned prior art reference.

EP Pat 0265111 A2 (D4) relates to the xylose production from the liquid portion of hydrolysis processes. This patent claims a processing the hydrolyzed liquid fraction of biomass. Again the product resulting from that patented process has clearly nothing to do with the solid catalytic cellulignin claimed in the present invention.

In fact, EP Pat 0265111 refers to the solid portion as an "insoluble residue", which is disposed of. There is no further consideration (technology) regarding the "solid residue". The fact that the solid portion is considered only as a residue in this patent as well as in most of earlier prior art patents relating to pre-hydrolysis process is the reason why up to the present invention there had been no optimization of the process conditions and parameters with the purpose of obtaining a fuel with the now claimed specific characteristics.

In present case, the inventors have taken a diametrically opposed way, that is to say, they have achieved improved conditions for the pre-hydrolysis process which allowed the obtention of a solid product with macromolecular porosity characteristics typical of a catalytic fuel. In other words, according to the present invention, the parameters such as time, temperature, acidic contents, stirring, hydric module (liquid contents/solid contents ratio) were optimized in order to yield a new and different resulting product that is composed of cellulose and globulized cellulignin with the specific surface of about 1.5 to 2.5 m<sup>2</sup>/g.

The resulting cellulignin according to the present invention is porous at macromolecular level, demineralized, friable, able to be ground down to submetric particles with low consumption of energy, easily dryable with the residual heat from the combustion gases at 230° C in short periods of time simultaneously with the grinding. These characteristics are a result of the

In view of the clarifications presented above, applicant respectfully submits that the invention as now claimed is novel and inventive over the prior art represented by D1 to D4.



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Associado à A.B.A.P.I. pe3848epo

Finally it is also observed that the expression "celluliginin fuel" is indeed the most appropriate technical expression to identify the claimed product and as far as the applicant is aware, it will be promptly understood by any person skilled in the art. For this reason, no amendment was effected therein.

Very truly yours

Maria Carmen S. Brito

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# From the

INTERNATIONAL PRELIMINARY EXAMINING AUTHORITY

DANNEMANN, SIEMSEN, BIGLER & **IPANEMA MOREIRA** Rua Marques de Olinda 70, Botafogo Caixa Postal 2142 22251-040- Rio de Janeiro - RJ BRESIL

NOTIFICATION OF TRANSMITTAL THE INTERNATIONAL PRELIMINARY **EXAMINATION REPORT** 01

(PCT Rule 71.1)

Date of mailing (day/month/year)

02.10.2001

Applicant's or agent's file reference

PE-3848

IMPORTANT NOTIFICATION

International application No. PCT/BR00/00066

International filing date (day/month/year) 23/06/2000

Priority date (day/month/year)

23/06/1999

Applicant

RM MATERIAIS REFRATARIOS LTDA.

- 1. The applicant is hereby notified that this International Preliminary Examining Authority transmits herewith the international preliminary examination report and its annexes, if any, established on the international application.
- 2. A copy of the report and its annexes, if any, is being transmitted to the International Bureau for communication to all the elected Offices.
- 3. Where required by any of the elected Offices, the International Bureau will prepare an English translation of the report (but not of any annexes) and will transmit such translation to those Offices.

### 4. REMINDER

The applicant must enter the national phase before each elected Office by performing certain acts (filing translations and paying national fees) within 30 months from the priority date (or later in some Offices) (Article 39(1)) (see also the reminder sent by the International Bureau with Form PCT/IB/301).

Where a translation of the international application must be furnished to an elected Office, that translation must contain a translation of any annexes to the international preliminary examination report. It is the applicant's responsibility to prepare and furnish such translation directly to each elected Office concerned.

For further details on the applicable time limits and requirements of the elected Offices, see Volume II of the PCT Applicant's Guide.

Name and mailing address of the IPEA/

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Authorized officer

Ferro Vasconcelos, M



# PATENT COOPERATION TREATY

# **PCT**

# INTERNATIONAL PRELIMINARY EXAMINATION REPORT

(PCT Article 36 and Rule 70)

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Applicant's or a	gent's file reference	FOR FURTHER ACTION	See Notifi	cation of Transmittal of International ry Examination Report (Form PCT/IPEA/416)
PE-3848		FOR FORTHER ACTION	- Preminia	
nternational ap	plication No.	International filing date (day/mo	nth/year)	Priority date (day/month/year)
PCT/BR00/0	00066	23/06/2000		23/06/1999
International Pa C10L5/44	atent Classification (IPC) or n	ational classification and IPC	•	
Applicant RM MATER	IAIS REFRATARIOS L	TDA.		
This inte and is tra	rnational preliminary exar ansmitted to the applicant	nination report has been prepa according to Article 36.	red by this In	ternational Preliminary Examining Authority
		of 5 sheets, including this cove		
beer (see	n amended and are the base Rule 70.16 and Section	asis for this report and/or shee 607 of the Administrative Instr	s containing	ion, claims and/or drawings which have rectifications made before this Authority the PCT).
These a	nnexes consist of a total of	of sheets.		
 	<ul> <li>☒ Basis of the report</li> <li>☐ Priority</li> <li>☐ Non-establishment of</li> <li>☐ Lack of unity of invertigations</li> <li>☒ Reasoned statement citations and explanations</li> <li>☐ Certain documents of</li> <li>☒ Certain defects in the</li> </ul>	under Article 35(2) with regard tions suporting such statemen	l to novelty, ir t	ep and industrial applicability nventive step or industrial applicability;
Date of subm	ission of the demand	Dat	e of completion	of this report
22/01/2001	l	02.	10.2001	
Name and ma	ailing address of the internation	onal Aut	horized officer	SOM COM MOOR
	European Patent Office D-80298 Munich	Va	n Iddekinge,	, R
	Tel. +49 89 2399 - 0 Tx: 523	656 epmu d		20 200 8245

# INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No. PCT/BR00/00066

i.	Basi	s of the report		to the same fundament to					
1.	the re	With regard to the elements of the international application (Replacement sheets which have been furnished to the receiving Office in response to an invitation under Article 14 are referred to in this report as "originally filed" and are not annexed to this report since they do not contain amendments (Rules 70.16 and 70.17)):  Description, pages:							
	1-36		as originally filed						
	Clair	ms, No.:							
	1-8	-	as originally filed						
	Drav	wings, sheets:							
	1-11		as originally filed						
				• • • • •					
2.	With lang	regard to the <b>lan</b> quage in which the	guage, all the elements marked above were available or furnishe international application was filed, unless otherwise indicated un	d to this Authority in the der this item.					
	The	se elements were	available or furnished to this Authority in the following language:	, which is:					
		the language of a	translation furnished for the purposes of the international search	(under Rule 23.1(b)).					
		the language of p	ublication of the international application (under Rule 48.3(b)).						
		the language of a 55.2 and/or 55.3)	translation furnished for the purposes of international preliminary	examination (under Rule					
3	. With inte	n regard to any <b>nu</b> rnational prelimina	cleotide and/or amino acid sequence disclosed in the internation of the sequence listing examination was carried out on the basis of the sequence listing.	onal application, the ng:					
		contained in the i	nternational application in written form.						
			the international application in computer readable form.	•					
			uently to this Authority in written form.						
		furnished subsec	uently to this Authority in computer readable form.						
	The statement that the subsequently furnished written sequence listing does not go beyond the disclos the international application as filed has been furnished.								
		The statement the listing has been to	at the information recorded in computer readable form is identical umished.	I to the written sequence					
4	I. The	e amendments hav	ve resulted in the cancellation of:						
		the description,	pages:						
		the claims,	Nos.:						

# INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No. PCT/BR00/00066

						•
		the drawings,	sheets:	-		
5.		considered to go bey	ond the dis	sclosure a	ome of) the amendments had not been made, s as filed (Rule 70.2(c)):	
		(Any replacement sh report.)	eet contain	ing such	amendments must be referred to under item 1 a	and annexed to this
6.	Add	itional observations, i	f necessary	<b>/</b> :		
٧.	Rea cita	soned statement un tions and explanatio	der Article ons suppo	e 35(2) wi rting suc	ith regard to novelty, inventive step or indus h statement	trial applicability;
1.	Stat	tement				•
	Nov	velty (N)	Yes: No:	Claims Claims	1-8	
	Inve	entive step (IS)	Yes: No:	Claims Claims	1-8	

2. Citations and explanations see separate sheet

Industrial applicability (IA)

## VII. Certain defects in the international application

The following defects in the form or contents of the international application have been noted: see separate sheet

Claims 1-8

Claims

#### VIII. Certain observations on the international application

Yes:

No:

The following observations on the clarity of the claims, description, and drawings or on the question whether the claims are fully supported by the description, are made: see separate sheet

## **EXAMINATION REPORT - SEPARATE SHEET**

#### Re Item V

Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement

Reference is made to the following documents: 1).

D1=US-A-5338366

D2=GB-A-1569138

D3=US-A-5366558

D4=EP-A-265111

D5=Bioresource Technology, vol. 59 (1997), pages 129-136

- According to the present application the claimed fuel is prepared by treating 2). biomass with an acidic solution under influence of heat and pressure until the hemicellulose is converted into sugar (pre-hydrolysis of biomass) and then removing the sugar (by means of washing), see page 11, line 18 - page 12, line 5. The biomass can be any type of biomass such as wood, sugar cane bagasse, straw, vegetable residues, barks, grass, etc.
  - D1 describes treating biomass (sugar cane bagasse) with an acidic solution (mineral acid 0.5-3.0%) under influence of heat (250-350°F) and pressure (30-50 psig) until the hemicellulose is converted into sugar (pre-hydrolysis of biomass) and then removing the sugar (by means of washing), see claims 28, 29. The residue corresponds to the presently claimed catalytic cellulignin fuel.
  - D2 describes treating cellulosic agricultural by-products (alfalfa, wheat straw, rice straw) with an acidic solution (mineral acid 0.1-1.0%) under influence of heat (100-160°C) and pressure until the hemicellulose is converted into sugar (prehydrolysis of biomass) and then removing the sugar (by means of washing), see page 2, lines 42-57; page 6, lines 28-33; claims 1, 4-6, 8, 18. The residue corresponds to the presently claimed catalytic cellulignin fuel.
  - D4 describes treating lignocellulosic feedstocks (straw) with an acidic solution (mineral acid 0.5-5.0%) under influence of heat (100-150°C) and pressure until the hemicellulose is converted into sugar (pre-hydrolysis of biomass) and then removing the sugar (by means of washing), see claims 1, 4-6. The residue corresponds to the presently claimed catalytic cellulignin fuel.

- D5 describes treating lignocellulosic feedstocks (i.e. com stover, poplar and switchgrass) with an acidic solution (sulfuric acid 0.6, 0.9 and 1.2 wt.%) under influence of heat (140, 160, 180°C) and pressure until the hemicellulose is converted into sugar (pre-hydrolysis of biomass) and then removing the sugar (by means of washing), see D5: page 129, "Abstract"; pages 130-131, "METHODS".

Since D1, D2, D4 and D5 disclose the same process steps, the resulting product should be identical. Thus D1, D2, D4 and D5 disclose a fuel according to claims 1-8 of the application.

Therefore claim 1 and its dependent claims 2-8 do not fulfil the requirements of Article 33(2) PCT (novelty).

#### Re Item VII

### Certain defects in the international application

3). Contrary to the requirements of Rule 5.1(a)(ii) PCT, the relevant background art disclosed in the documents D1, D2 and D5 is not mentioned in the description, nor are these documents identified therein.

#### Re Item VIII

### Certain observations on the international application

4). The term "catalytic cellulignin fuel" used in claims 1-8 is vague and unclear and leaves the reader in doubt as to the meaning of the technical features to which it refers, thereby rendering the definition of the subject-matter of said claims unclear (Article 6 PCT).

From the:

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**BRESIL** 

WRITTEN OPINION

(PCT Rule 66)

	į			
		Date of mailing (day/month/year)	21.03.2001	
Applicant's or agent's file reference PE-3848		REPLY DUE	within 3 month(s) from the above date of mailing	
International application No. International filing date PCT/BR00/00066 23/06/2000		te (day/month/year) Priority date (day/month/year 23/06/1999		
International Patent Classification (IPC) or	both national classification a	nd IPC		
C10L5/44				
Applicant			• • •	
RM MATERIAIS REFRATARIOS	LTDA.			

1.	This written or	pinion is the <b>firs</b>	t drawn up by th	is International	Preliminary	Examining /	Authority
----	-----------------	---------------------------	------------------	------------------	-------------	-------------	-----------

- This opinion contains indications relating to the following items:
  - Basis of the opinion
  - **Priority** 11
  - Non-establishment of opinion with regard to novelty, inventive step and industrial applicability III
  - Lack of unity of invention IV
  - Reasoned statement under Rule 66.2(a)(ii) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement
  - VI Certain document cited
  - $\boxtimes$ Certain defects in the international application VII
  - ☑ Certain observations on the international application VIII
- The applicant is hereby invited to reply to this opinion.
  - See the time limit indicated above. The applicant may, before the expiration of that time limit, When?

request this Authority to grant an extension, see Rule 66.2(d).

By submitting a written reply, accompanied, where appropriate, by amendments, according to Rule 66.3. How?

For the form and the language of the amendments, see Rules 66.8 and 66.9.

For an additional opportunity to submit amendments, see Rule 66.4. Also:

For the examiner's obligation to consider amendments and/or arguments, see Rule 66.4 bis.

For an informal communication with the examiner, see Rule 66.6.

If no reply is filed, the international preliminary examination report will be established on the basis of this opinion.

The final date by which the international preliminary examination report must be established according to Rule 69.2 is: 23/10/2001.

Name and mailing address of the international preliminary examining authority:

**European Patent Office** D-80298 Munich

Tel. +49 89 2399 - 0 Tx: 523656 epmu d

Fax: +49 89 2399 - 4465

Authorized officer / Examiner

Van Iddekinge, R

Formalities officer (incl. extension of time limits)

Christensen, J Telephone No. +49 89 2399 8052



## WRITTEN OPINION

i. Ba	asis	of	the	opi	inion
-------	------	----	-----	-----	-------

		•			
•	This in re	opinion has been o sponse to an invita	drawn on the basis of ( tion under Article 14 au	substitute sheets which have been fumisl re referred to in this opinion as "originally t	ned to the receiving Office filed".):
	Desc	cription, pages:			•
	1-36	,	as originally filed		
-	Claiı	ms, No.:			
	1-8		as originally filed		
	Drav	wings, sheets:	·		
	1-11		as originally filed		:
2.	lang	uage in which the	international application	s marked above were available or furnishe on was filed, unless otherwise indicated un to this Authority in the following language:	der mis item.
		<del>-</del> -		or the purposes of the international search	(under Hule 23.1(b)).
				ational application (under Rule 48.3(b)).	
		the language of a 55.2 and/or 55.3).		or the purposes of international preliminar	y examination (under hule
3.	With	n regard to any nuc mational prelimina	cleotide and/or amino ry examination was car	acid sequence disclosed in the internation of the sequence listing the s	onal application, the ng:
		contained in the ir	nternational application	in written form.	
				cation in computer readable form.	.*
		furnished subsequ	ently to this Authority	in written form.	
				in computer readable form.	
		The statement that the international a	at the subsequently fun application as filed has	nished written sequence listing does not g been furnished.	jo beyond the disclosure in
			at the information recor	rded in computer readable form is identica	I to the written sequence
4.	The	· ·	e resulted in the cance	ellation of:	
		the description,	pages:		
		the claims,	Nos.:		
		are country			

#### WRITTEN OPINION

		the drawings,	sheets:
5. 🗆		This report has been considered to go bey	established as if (some of) the amendments had not been made, since they have been yound the disclosure as filed (Rule 70.2(c)):
		(Any replacement sh report.)	neet containing such amendments must be referred to under item 1 and annexed to this

- 6. Additional observations, if necessary:
- V. Reasoned statement under Rule 66.2(a)(ii) with regard to novelty, inventive step or industrialapplicability; citations and explanations supporting such statement
- 1. Statement

Novelty (N)

Claims 1-8

Inventive step (IS)

Claims 1-8

Industrial applicability (IA)

Claims

- 2. Citations and explanations see separate sheet
- VII. Certain defects in the international application

The following defects in the form or contents of the international application have been noted: see separate sheet

#### VIII. Certain observations on the international application

The following observations on the clarity of the claims, description, and drawings or on the question whether the claims are fully supported by the description, are made: see separate sheet

#### WRITTEN OPINION SEPARATE SHEET

#### Re Item V

Reasoned statement under Rule 66.2(a)(ii) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement

International application No.

1). Reference is made to the following documents:

D1=US-A-5338366 D2=GB-A-1569138 D3=US-A-5366558

D4=EP-A-265111

 According to the present application the claimed fuel is prepared by treating biomass with an acidic solution under influence of heat and pressure until the hemicellulose is converted into sugar and then removing the sugar (by means of washing), see page 11, line 18 - page 12, line 5.

Since D1, D2, D3 and D4 disclose the same process steps, the resulting product should be identical, see D1: column 5, lines 27-39; claims 27-29 and D2: claim 1 and D3: claim 1 and D4: claim 1; page 2, line 41-page 3, line 4.

Therefore claim 1 and its dependent claims 2-8 do not fulfil the requirements of Article 33(2) PCT (novelty).

If the applicant does not agree with the novelty objection, the applicant should indicate in the letter of reply the difference of the subject-matter of the claims vis-à-vis the state of the art (product features of the claims not disclosed in the prior art) and the significance thereof for the inventive step.

#### Re Item VII

## Certain defects in the international application

 Contrary to the requirements of Rule 5.1(a)(ii) PCT, the relevant background art disclosed in the documents D1 and D2 is not mentioned in the description, nor are these documents identified therein.

#### International application No.

#### Re Item VIII

## Certain observations on the international application

4). The term "catalytic cellulignin fuel" used in claims 1-8 is vague and unclear and leaves the reader in doubt as to the meaning of the technical features to which it refers, thereby rendering the definition of the subject-matter of said claims unclear (Article 6 PCT).

The demand must be filed directly with the competent International Preliminary Examining Authority and two or more Authorities are competent, with the one chosen by the applicant. The full name or two-letter code of that Authority may be indicated by the applicant on the line below:

TPEA/ EPO

## **PCT**

**CHAPTER II** 

#### **DEMAND**

under Article 31 of the Patent Cooperation Treaty:

The undersigned requests that the international application specified below be the subject of international preliminary examination according to the Patent Cooperation Treaty and hereby elects all eligible States (except where otherwise indicated).

For	International Preliminary	Examining Authority	y use only		
· · · · · · · · · · · · · · · · · · ·	·	Date of receipt of D	DEMAND		
lentification of IPEA			Applicant's or agent's file reference		
ox No. I DENTIFICATION OF T	HE INTERNATIONAL	APPLICATION	PE-3848		
nternational application No.	International filing date	(day/month/year)	(Earliest) Priority date (day/month/year) 23 June 1999		
PCT/BR00/00066	23 June 200 (23.06.2000		(23.06.99)		
itle of invention "CATALYTIC CELLULIGE	NIN FUEL"				
ox No. II APPLICANT(S)					
Name and address: (Family name followed by given name; for a legal entity, full official designation.  The address must include postal code and name of country.)  The coddress must include postal code and name of country.)					
RM MATERIAIS REFRATA	RIOS LTDA.		Facsimile No.:		
Estrada do Pinhal, 7 12600-000 - Lorena -	SP	-			
Brazil			Teleprinter No.:		
·					
State (that is, country) of nationality:	BR	State (that is, cour BF			
Name and address: (Family name followed by	y given name; for a legal entity,	full official designation. T	he address must include postal code and name of country.		
GARCIA PINATTI, DALT Rua Oswaldo Aranha,	'RO				
Vila Zelia Lorena, São Paulo					
Brazil					
State (that is, country) of nationality:	BR	State (that is, cou	intry) of residence:		
Name and addresses (Family some followed	by given name: for a legal entity	, full official designation. I	The address must include postal code and name of country		
VIEIRA, CHRISTIAN AL Av. Andrade Neves,	LEXANDRE				
Centro Campinas, São Paulo Brazil					
			ntry) of residence:		

Sheet No. .02

International application No. PCT/BR00/00066

Continuation of Box No. II APPLICANT(S)					
If none of the following sub-boxes is used, this sheet should not be included in the demand.					
Name and address: (Family name followed by given name; for a legal end	tity, full official designation. The address must include postal code and name of country:)				
GUEDES SOARES, ALVARO Rua Madre Amanda de Castro Junqu Mirante Mogi Mirim, São Paulo Brazil	ueira, 117				
	State (that is, country) of residence:				
State (that is, country) of nationality: BR	BR				
Name and address: (Family name followed by given name; for a legal et	ntity, full official designation. The address must include postal code and name of country.)				
•					
·					
State (that is, country) of nationality:	State (that is, country) of residence:				
I delegate (Family name followed by given name; for a legal e	nitry, full official designation. The address must include postal code and name of country.)				
Name and address. (1 may none years)					
	_				
	State (that is, country) of residence:				
State (that is, country) of nationality:					
Name and address: (Family name followed by given name: for a legal	entity, full official designation. The address must include postal code and name of country.)				
·					
	•				
State (that is, country) of nationality:	State (that is, country) of residence:				
	tion sheet.				
Further applicants are indicated on another continua	San Notes to the demand for				

Sheet No. 03

International application No.
PCT/BR00/00066

Box No. III AGENT OR COMMON REPRESENTATIVE; OR ADDRESS FOR CORRESPONDENCE					
The following person is x agent common representative					
and has been appointed earlier and represents the applicant(s) also for international pre	liminary examination.				
is hereby appointed and any earlier appointment of (an) agent(s)/common represent	tative is hereby revoked.				
is hereby appointed, specifically for the procedure before the International Prelimi	nary Examining Authority, in addition to				
is hereby appointed, specifically for the procedure below the agent(s)/common representative appointed earlier.					
(Emily and followed by given name: for a legal entity, full official designation.	Telephone No.:				
The dual ess mass minimum poor	(5521) 553.1811				
DANNEMANN, SIEMSEN, BIGLER & IPANEMA MOREIRA					
Caixa Postal 2142	Facsimile No.: (5521) 553.1812				
Rua Marquês de Olinda, 70 Botafogo	553.1813				
22251-040 - Rio de Janeiro - RJ	Teleprinter No.:				
Brazil					
Address for correspondence: Mark this check-box where no agent or common re	presentative is/has been appointed and the				
space above is used instead to indicate a special and less to which correspondent	should be sent.				
Box No. IV BASIS FOR INTERNATIONAL PRELIMINARY EXAMINATION					
Statement concerning amendments:*					
1. The applicant wishes the international preliminary examination to start on the basis of					
x the international application as originally filed					
the description X as originally filed					
as amended under Article 34					
the claims x as originally filed					
as amended under Article 19 (together with any accompanying	g statement)				
as amended under Article 34					
the drawings X as originally filed	_				
as amended under Article 34					
2. The applicant wishes any amendment to the claims under Article 19 to be consider	rred as reversed.				
3. The applicant wishes the start of the international preliminary examination to be p from the priority date unless the International Preliminary Examining Authority	receives a copy of any amendments made				
under Article 19 or a notice from the applicant that he does not wish to make such box may be marked only where the time limit under Article 19 has not yet expired	amendments (Kule 69.1(d)). (Inis check-				
* When so shock how is marked international preliminary examination will start on	the basis of the international application				
as originally filed or, where a copy of amendments to the claims under Article 19 and/or amendments of the international application under Article 34 are received by the International Preliminary Examining Authority before it has begun to draw up a written opinion or the international preliminary examination report, as so amended.					
Language for the purposes of international preliminary examination: English					
which is the language in which the international application was filed.					
which is the language of a translation furnished for the purposes of international search.					
which is the language of publication of the international application.					
which is the language of the translation (to be) furnished for the purposes of international preliminary examination.					
Box No. V ELECTION OF STATES					
The applicant hereby elects all eligible States (that is, all States which have been designated	ted and which are bound by Chapter II of				
the PCT) excluding the following States which the applicant wishes not to elect:					
excluding the following states which the applicant wishes not to elect.	!				

Sheet No. .04

International application No. PCT/BR00/00066

Box No. VI CHECK LIST				
The demand is accompanied by the following elements, in the language referred to in			For International Examining	ational Preliminary Authority use only
Box No. IV, for the purposes of international	The demand is accompanied by the following obstitutions:  Box No. IV, for the purposes of international preliminary examination:			not received
1. translation of international application	:	sheets		
2. amendments under Article 34	:	sheets		
copy (or, where required, translation) of amendments under Article 19	:	sheets		
copy (or, where required, translation) of statement under Article 19	:	sheets		
	:	sheets		
5. letter	:	sheets		
6. other (specify)				
The demand is also accompanied by the item(s)	marked below:		at explaining lack of s	ionature
1.		L	de and or amino acid	i.
2. separate signed power of attorney			r readable form	·
3. copy of general power of attorney, reference number, if any:		6. other (sp	pecify): 	
Box No. VII SIGNATURE OF APPLICANT	, AGENT OR	COMMON REPRE	SENTATIVE	
Next to each signature, indicate the name of the person sign	ing and the capacity	in which the person signs (	if such capacity is not obvio	nus from reading the demand).
				·
Dannemann, Siemsen, Bi	mid = 0 Tr	nanema More	ra	
Dannemann, Siemsen, Bi	dier a T	panema Hore.		-
For Intern	ational Prelimina	ary Examining Author	ity use only	
Date of actual receipt of DEMAND:				
Adjusted date of receipt of demand due     to CORRECTIONS under Rule 60.1(b):				
The date of receipt of the demand is AFTER the expiration of 19 months from the priority date and item 4 or 5, below, does not apply.  The applicant has been informed accordingly.				
4. The date of receipt of the demand is WITHIN the period of 19 months from the priority date as extended by virtue of Rule 80.5.				
5. Although the date of receipt of the demand is after the expiration of 19 months from the priority date, the delay in arrival is EXCUSED pursuant to Rule 82.				
	- For Internati	onal Bureau use only		
Demand received from IPEA on:				

## **PCT**

#### FEE CALCULATION SHEET

## Annex to the Demand for international preliminary examination

	For International Preliminary Examining Authority use only			
International application No. PCT/BR00/00066	, i			
Applicant's or agent's file reference PE-3848	Date stamp of the IPEA			
Applicant				
RM MATERIAIS REFRATÁRIOS LTDA.				
Calculation of prescribed fees				
1. Preliminary examination fee	DEM 749,58 P			
2. Handling fee (Applicants from certain States are entitled to a reduction of 75% of the handling fee. Where the applicant is (or all applicants are) so entitled, the amount to be entered at H is 25% of the handling fee.)	DEM 287.51 H			
3. Total of prescribed fees Add the amounts entered at P and H and enter total in the TOTAL box	EM 1.037.09 TOTAL			
Mode of Payment  authorization to charge deposit account with the IPEA (see below)  cheque revenue  postal money order coupons  bank draft other (s)	S			
Deposit Account Authorization (this mode of payment may not be available at all IPEAs)  The IPEA/ is hereby authorized to charge the total fees indicated above to my deposit account.  (this check-box may be marked only if the conditions for deposit accounts of the IPEA so permit) is hereby authorized to charge any deficiency or credit any overpayment in the total fees indicated above to my deposit account.				
Deposit Account Number Date (day/month/year)	Signature			

#### From the: INTERNATIONAL PRELIMINARY EXAMINING AUTHORITY

To:

DANNEMANN, SIEMSEN, BIGLER & IPANEMA MOREIRA Rua Marques de Olinda 70, Botafogo Caixa Postal 2142 22251-040- Rio de Janeiro - RJ BRESIL

10-9-0

WRITTEN OPINI

(PCT Rule 66)

Date of mailing (day/month/year)

**REPLY DUE** 

10.07.2001

Applicant's or agent's file reference

PE-3848

within 2 month(s)

Priority date (day/month/year)

from the above date of mailing

International application No.

PCT/BR00/00066

International filing date (day/month/year)

23/06/2000

23/06/1999

International Patent Classification (IPC) or both national classification and IPC

C10L5/44

II

Applicant

RM MATERIAIS REFRATARIOS LTDA.

- This written opinion is the second drawn up by this International Preliminary Examining Authority.
- This opinion contains indications relating to the following items:
  - Basis of the opinion
    - Priority
  - Non-establishment of opinion with regard to novelty, inventive step and industrial applicability Ш
  - IV Lack of unity of invention
    - Reasoned statement under Rule 66.2(a)(ii) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement
  - VI Certain document cited
  - VII Certain defects in the international application
  - Certain observations on the international application VIII
- The applicant is hereby invited to reply to this opinion.

See the time limit indicated above. The applicant may, before the expiration of that time limit, When?

request this Authority to grant an extension, see Rule 66.2(d).

By submitting a written reply, accompanied, where appropriate, by amendments, according to Rule 66.3. How?

For the form and the language of the amendments, see Rules 66.8 and 66.9.

Also: For an additional opportunity to submit amendments, see Rule 66.4.

For the examiner's obligation to consider amendments and/or arguments, see Rule 66.4 bis.

For an informal communication with the examiner, see Rule 66.6.

If no reply is filed, the international preliminary examination report will be established on the basis of this opinion.

The final date by which the international preliminary examination report must be established according to Rule 69.2 is: 23/10/2001.

Name and mailing address of the international preliminary examining authority:

**European Patent Office** D-80298 Munich

Tel. +49 89 2399 - 0 Tx: 523656 epmu d

Fax: +49 89 2399 - 4465

Authorized officer / Examiner

Van Iddekinge, R

Formalities officer (incl. extension of time limits)

Gregoire, J-P

Telephone No. +49 89 2399 8041



#### **WRITTEN OPINION**

l. Basis	of the	e opini	on
----------	--------	---------	----

1.			nents of the international application (Replacement <i>Sheets Whic</i> response to an invitation under Article 14 are referred to in this o		
	Des	scription, pages:			
	1-3	6	as originally filed		
	Cla	ims, No.:			÷
	1-8		as originally filed		
	Dra	wings, sheets:			
	1-1	1	as originally filed		
2.			juage, all the elements marked above were available or furnishe international application was filed, unless otherwise indicated un		y in the
	The	ese elements were a	available or furnished to this Authority in the following language:	, which is:	•
		the language of a	translation furnished for the purposes of the international search	ı (under Rule 23.1	l(b)).
		the language of pu	ublication of the international application (under Rule 48.3(b)).		
		the language of a 55.2 and/or 55.3).	translation furnished for the purposes of international preliminary	y examination (un	der Rule
3.		•	eleotide and/or amino acid sequence disclosed in the internation was carried out on the basis of the sequence listing	• •	he
		contained in the in	ternational application in written form.		•
		filed together with	the international application in computer readable form.		
		furnished subsequ	ently to this Authority in written form.	•	
		furnished subsequ	ently to this Authority in computer readable form.		
			t the subsequently furnished written sequence listing does not gopplication as filed has been furnished.	o beyond the disc	losure in
		The statement tha listing has been fu	t the information recorded in computer readable form is identical mished.	to the written sec	quence
1.	The	amendments have	resulted in the cancellation of:	:7	
		the description,	pages:		
		the claims,	Nos.:		

WRITTEN OPINION

International application No. PCT/BR00/00066

		the drawings,	sheets:	
5.		This report has been considered to go bey	established as if (some of) the amendments had not been made, since they have been ond the disclosure as filed (Rule 70.2(c)):	÷n
		(Any replacement sh report.)	eet containing such amendments must be referred to under item 1 and annexed to thi	s
6.	Add	itional observations, i	necessary:	

- V. Reasoned statement under Rule 66.2(a)(ii) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement
- 1. Statement

Novelty (N)

Claims 1-8

Inventive step (IS)

Claims 1-8

Industrial applicability (IA)

Claims

2. Citations and explanations see separate sheet

#### VII. Certain defects in the international application

The following defects in the form or contents of the international application have been noted: see separate sheet

#### VIII. Certain observations on the international application

The following observations on the clarity of the claims, description, and drawings or on the question whether the claims are fully supported by the description, are made: see separate sheet

#### Re Item V

Reasoned statement under Rule 66.2(a)(ii) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement

- 1). According to the applicant (letter of 20.06.2001) the claimed catalytic cellulignin fuel product is novel because D1, D2, D3 and D4 disclose a different production process.
- 2). According to the present application the claimed fuel is prepared by treating biomass with an acidic solution under influence of heat and pressure until the hemicellulose is converted into sugar (pre-hydrolysis of biomass) and then removing the sugar (by means of washing), see page 11, line 18 page 12, line 5. The biomass can be any type of biomass such as wood, sugar cane bagasse, straw, vegetable residues, barks, grass, etc.

In D1 sugar cane bagasse is treated with an acidic solution (mineral acid 0.5-3.0%) under influence of heat (250-350°F) and pressure (30-50 psig) until the hemicellulose is converted into sugar (pre-hydrolysis of biomass) and then removing the sugar (by means of washing), see claims 28, 29. The residue corresponds to the presently claimed catalytic cellulignin fuel.

In D2 straw is treated with an acidic solution (mineral acid 0.1-1.0%) under influence of heat (100-160°C) and pressure until the hemicellulose is converted into sugar (pre-hydrolysis of biomass) and then removing the sugar (by means of washing), see page 2, lines 42-57; page 6, lines 28-33; claims 1, 4-6, 8, 18. The residue corresponds to the presently claimed catalytic cellulignin fuel.

In D4 straw is treated with an acidic solution (mineral acid 0.5-5.0%) under influence of heat (100-150°C) and pressure until the hemicellulose is converted into sugar (pre-hydrolysis of biomass) and then removing the sugar (by means of washing), see claims 1, 4-6. The residue corresponds to the presently claimed catalytic cellulignin fuel.

Thus the novelty objection in view of D1, D2 and D4 is maintained.

Therefore claim 1 and its dependent claims 2-8 do not fulfil the requirements of Article 33(2) PCT (novelty).

If the applicant does not agree with the novelty objection, the applicant should indicate in the letter of reply the difference of the subject-matter of the claims vis-à-vis the state of the art (product features of the claims not disclosed in the prior art) and the significance thereof for the inventive step.

It is to be noted that D5 (Bioresource Technology, vol. 59 (1997), pages 129-136) also discloses the presently claimed catalytic cellulignin fuel.

#### Re Item VII

## Certain defects in the international application

Contrary to the requirements of Rule 5.1(a)(ii) PCT, the relevant background art 3). disclosed in the documents D1 and D2 is not mentioned in the description, nor are these documents identified therein.

#### Re Item VIII

## Certain observations on the international application

The term "catalytic cellulignin fuel" used in claims 1-8 is vague and unclear and 4). leaves the reader in doubt as to the meaning of the technical features to which it refers, thereby rendering the definition of the subject-matter of said claims unclear (Article 6 PCT).

If the applicant is of the opinion that the term "catalytic cellulignin fuel" used in claims 1-8 is well known and clear, the applicant should prove this by sending a copy of a document (or book) giving a definition of this term.

**PCT** 

REC'D 0 4 OCT 2001

## INTERNATIONAL PRELIMINARY EXAMINATION REPORTET

(PCT Article 36 and Rule 70)

Applicant's	s or aq	ent's file reference		0 N	NE A Transition of Transition
PE-3848			FOR FURTHER A	ATIALI	otification of Transmittal of International inary Examination Report (Form PCT/IPEA/416)
Internation	nat app	lication No.	International filing date (	day/month/year)	Priority date (day/month/year)
PCT/BR	00/00	0066	23/06/2000		23/06/1999
Internation C10L5/4		ent Classification (IPC) or n	ational classification and IP	С	
Applicant	reri <i>i</i>	AIS REFRATARIOS L	TDA.		·
			nination report has been according to Article 36.	prepared by this	International Preliminary Examining Authority
2. This	REPO	ORT consists of a total o	f 5 sheets, including this	s cover sheet.	<u>:</u>
t (	seen a	mended and are the ba	sis for this report and/or 607 of the Administrative	sheets containin	ption, claims and/or drawings which have g rectifications made before this Authority er the PCT).
3. This	report	contains indications rel	ating to the following iter	ns:	
I	$\boxtimes$	Basis of the report			
11		Priority			
111				velty, inventive s	tep and industrial applicability
IV	_	Lack of unity of invent			
V	×		under Article 35(2) with re ions suporting such state		inventive step or industrial applicability;
VI		Certain documents cit	ted .		•
VII	$\boxtimes$	Certain defects in the	international application		
VIII	⊠	Certain observations of	on the international applic	cation	
Date of sul	bmissio	on of the demand		Date of completio	n of this report
22/01/20	001			02.10.2001	
		g address of the internation ining authority:	al	Authorized officer	SPONSONS MILITARY
<i>(</i> )	Euro D-80	opean Patent Office 0298 Munich +49 89 2399 - 0 Tx: 52365	S comu d	Van Iddekinge	e, R
		+49 89 2399 - 4465	o spiliu u	Telenhone No. +4	0.90.2200.9246





International application No. PCT/BR00/00066

I. Basis of the report

1.	the and	receiving Office in I	response to an invitation under Article 14 are referred to in this report as "originally filed" this report since they do not contain amendments (Rules 70.16 and 70.17)):
	1-3	6	as originally filed
	Cla	ims, No.:	
	1-8		as originally filed
	Dra	wings, sheets:	
	1-1	1	as originally filed
2.		•	uage, all the elements marked above were available or furnished to this Authority in the nternational application was filed, unless otherwise indicated under this item.
	The	se elements were a	vailable or furnished to this Authority in the following language: , which is:
		the language of a t	ranslation furnished for the purposes of the international search (under Rule 23.1(b)).
		the language of pu	blication of the international application (under Rule 48.3(b)).
		the language of a t 55.2 and/or 55.3).	ranslation furnished for the purposes of international preliminary examination (under Rule
3.			leotide and/or amino acid sequence disclosed in the international application, the y examination was carried out on the basis of the sequence listing:
		contained in the int	ternational application in written form.
		filed together with t	the international application in computer readable form.
		furnished subsequ	ently to this Authority in written form.
		furnished subsequ	ently to this Authority in computer readable form.
			the subsequently furnished written sequence listing does not go beyond the disclosure in oplication as filed has been furnished.
		The statement that listing has been ful	the information recorded in computer readable form is identical to the written sequence rnished.
4.	The	amendments have	resulted in the cancellation of:
		the description,	pages:
		the claims,	Nos.:





**EXAMINATION REPORT** International application No. PCT/BR00/00066

		the drawings,	sheets:		
5.					some of) the amendments had not been made, since they have bee as filed (Rule 70.2(c)):
		(Any replacement shoreport.)	eet contai	ning such	h amendments must be referred to under item 1 and annexed to this
6.	Add	litional observations, if	necessar	y:	
V.				e 35(2) w	with regard to novelty, inventive step or industrial applicability;
		itions and explanatio	ns suppo	rting suc	ch statement
1.		tement	ns suppo	rting suc	ch statement
1.	Stat	•	ns suppo Yes: No:	Claims Claims	
1.	Stat Nov	tement	Yes:	Claims Claims	1-8

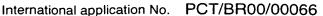
2. Citations and explanations see separate sheet

#### VII. Certain defects in the international application

The following defects in the form or contents of the international application have been noted: see separate sheet

#### VIII. Certain observations on the international application

The following observations on the clarity of the claims, description, and drawings or on the question whether the claims are fully supported by the description, are made: see separate sheet



#### **EXAMINATION REPORT - SEPARATE SHEET**

#### Re Item V

Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement

Reference is made to the following documents: 1).

D1=US-A-5338366

D2=GB-A-1569138

D3=US-A-5366558

D4=EP-A-265111

D5=Bioresource Technology, vol. 59 (1997), pages 129-136

- According to the present application the claimed fuel is prepared by treating 2). biomass with an acidic solution under influence of heat and pressure until the hemicellulose is converted into sugar (pre-hydrolysis of biomass) and then removing the sugar (by means of washing), see page 11, line 18 - page 12, line 5. The biomass can be any type of biomass such as wood, sugar cane bagasse, straw, vegetable residues, barks, grass, etc.
  - D1 describes treating biomass (sugar cane bagasse) with an acidic solution (mineral acid 0.5-3.0%) under influence of heat (250-350°F) and pressure (30-50 psig) until the hemicellulose is converted into sugar (pre-hydrolysis of biomass) and then removing the sugar (by means of washing), see claims 28, 29. The residue corresponds to the presently claimed catalytic cellulignin fuel.
  - D2 describes treating cellulosic agricultural by-products (alfalfa, wheat straw, rice straw) with an acidic solution (mineral acid 0.1-1.0%) under influence of heat (100-160°C) and pressure until the hemicellulose is converted into sugar (prehydrolysis of biomass) and then removing the sugar (by means of washing), see page 2, lines 42-57; page 6, lines 28-33; claims 1, 4-6, 8, 18. The residue corresponds to the presently claimed catalytic cellulignin fuel.
  - D4 describes treating lignocellulosic feedstocks (straw) with an acidic solution (mineral acid 0.5-5.0%) under influence of heat (100-150°C) and pressure until the hemicellulose is converted into sugar (pre-hydrolysis of biomass) and then removing the sugar (by means of washing), see claims 1, 4-6. The residue corresponds to the presently claimed catalytic cellulignin fuel.

- D5 describes treating lignocellulosic feedstocks (i.e. corn stover, poplar and switchgrass) with an acidic solution (sulfuric acid 0.6, 0.9 and 1.2 wt.%) under influence of heat (140, 160, 180°C) and pressure until the hemicellulose is converted into sugar (pre-hydrolysis of biomass) and then removing the sugar (by means of washing), see D5: page 129, "Abstract"; pages 130-131, "METHODS".

Since D1, D2, D4 and D5 disclose the same process steps, the resulting product should be identical. Thus D1, D2, D4 and D5 disclose a fuel according to claims 1-8 of the application.

Therefore claim 1 and its dependent claims 2-8 do not fulfil the requirements of Article 33(2) PCT (novelty).

#### Re Item VII

#### Certain defects in the international application

Contrary to the requirements of Rule 5.1(a)(ii) PCT, the relevant background art 3). disclosed in the documents D1, D2 and D5 is not mentioned in the description, nor are these documents identified therein.

#### Re Item VIII

#### Certain observations on the international application

4). The term "catalytic cellulignin fuel" used in claims 1-8 is vague and unclear and leaves the reader in doubt as to the meaning of the technical features to which it refers, thereby rendering the definition of the subject-matter of said claims unclear (Article 6 PCT).